

May 21, 2024

Fremont County Department of Planning and Zoning Attn: Dan Victoria 615 Macon Avenue, Room 210 Canon City, CO 81212

RE: CDP Re-Review – Penrose RV & Boat Storage, 17225 SH 115, Penrose, CO

Hello Mr. Victoria,

Please find included for your re-review of the above-mentioned project the following amended documents:

- 1. Revised CDP Application, referencing updates to the project, which include the following:
 - a. Removal of Caretaker's Unit, therefore the removal of the associated design facets:
 - i. Septic System
 - ii. Parking
 - iii. Site lighting references
 - b. Removal of Site Fencing on the exterior perimeter of the property
 - c. Addition of a locking hose bib for Ownership-only use
- 2. Revised Drainage Report
- 3. Revised Water Demand Memo
- 4. Revised Water Resources Form
- 5. Revised Project Narrative
- 6. Revised Civil Construction Drawings
- 7. Project Perspectives

Our hope is that with a standard two week review cycle, we will be able to meet the deadline to submit to BOZA by June 10th for the June 18th meeting.

Thank you in advance for your time and consideration.

Nicole Suttle Preconstruction Project Engineer



FREMONT COUNTY DEPARTMENT OF PLANNING AND ZONING

615 MACON AVENUE, ROOM 210, CAÑON CITY, COLORADO, 81212 Telephone 719-276-7360 / Facsimile 719-276-7374 Email: <u>Planning@fremontco.com</u>

LAND USE APPLICATION

SPECIAL REVIEW USE, CONDITIONAL USE PERMIT, COMMERCIAL DEVELOPMENT PLAN

It is recommended that the applicant schedule an appointment with a Department of Planning & Zoning Representative prior to application preparation and submittal to discuss the project as currently planned and future project proposals.

| Project Name: Penrose RV & Boat Storage |
|--|
| Site Address: 17225 SH 115, Penrose, CO 81240 |
| Applicant(s) |
| Name(s) Anna Fluckey |
| Address 650 Innovation Cir., Windsor, CO 80550 |
| Phone <u>970-686-6300</u> Fax |
| Email anna.fluckey@mccauleyconstructors.com |
| <u>Owner(s)</u> |
| Name(s) John Edgar, EPCOCO REI One, LLC |
| Address 3455 Fillmore Heights, Colorado Springs, CO 80907 |
| Phone <u>719-651-5563</u> Fax |
| Email john@edgartruck.com |
| Authorized Representative / Agent / Consultant (if other than owner) |
| Name(s) <u>Anna Fluckey</u> |
| Address 650 Innovation Cir., Windsor, CO 80550 |
| Phone <u>970-686-6300</u> Fax |
| Email_anna.fluckey@mccauleyconstructors.com |
| |

Type of Application / Application Fee (There maybe additional fees for publications or professional reviews):

□Special Review Use Permit \$1,800 □Major Modification to existing permit \$500

□Conditional Use Permit \$1,750 □Major Modification to existing permit \$500

Commercial Development Plan \$1750 Major Modification \$500

The applicant shall provide **one (1) original document, and an electronic copy (either CD or flash/thumb drive) of the application**, site plan (**2 COPIES**) and all of its attachments (*copies of deeds, contracts, leases etcetera are acceptable*) at the time of application submittal along with the **application fee** set as per Resolution of the Board. Submittals shall be made to the Department <u>no later than 3:00 pm</u> on the submittal deadline date.

Process & Requirements Overview

Any application which is not complete or does not include all minimum submittal requirements will be rejected by the Fremont County Department of Planning and Zoning (Department). Further, any application that is inadequate or incomplete, may be subject to postponement of placement on an agenda of the Fremont County Planning Commission (Commission), pending receipt of an adequate and complete application.

Upon receipt of a complete application, the Department will review the application and all attachments and prepare a Department Submittal Deficiency and Comment Letter (D & C Letter), which will state the submittal deficiencies which must be addressed by the applicant, Department comments and/or questions about the application, and the number of revised application packets to be supplied to the Department for placement on an agenda of the Commission. An additional full application fee may be charged to the applicant, as per Resolution approved by the Board of County Commissioners (Board), if all deficiencies as per the initial D & C Letter are not adequately addressed or provided. Each subsequent D & C Letter, based on resubmitted items, will result in another full application fee. All such fees shall be paid along with the deficiency submittal, prior to any further review of the application.

The Department, Commission, and/or Board may require additional information at any time during the application process as may be deemed necessary for thorough consideration of the application and to enable an informed final decision.

Any Land Use application for that has been submitted after the use requiring the permit has been established on the property may be subject to a penalty fee in addition to the set application fee for such permit. The penalty fee shall be equal to the initial application fee for the Land Use Application. As with all land use applications payment of associated fees <u>do not ensure approval</u> of the application.

If the application is approved by the Board with contingencies the contingencies shall be completed to the Department within six (6) months of the approval date, or the approval shall be deemed rescinded and the application expired, after which, re-submittal of the application, including fees, and procedural requirements, will be required.

In approving an application for Land Use, the Board may require higher standards for development than required by the Fremont County Zoning Resolution (FCZR).

Modifications, major or minor, to the Land Use Permit as approved, shall be accomplished in compliance with requirements of the Fremont County Zoning Resolution.

Applicants shall pay all application fees to the Fremont County Treasurer's Office. Upon receipt of a complete application, a Department representative will provide the applicant with a payment check list to present to the Treasurer's Office with payment.

Site & Development

(Section 1)

1. Describe the proposed type of operation to include days & hours of operation, number of employees, & machinery:

New ground-up Pre-Engineered Metal building (PEMB) erected for the purposes of a new commercial RV & Boat Storage

Facility. This facility is strictly Self-Storage, open to customers approximately 365 days each year, no on-site services.

Tenancy established through telephone and email communication and documentation only.

- 2. Property address or schedule number: <u>17225 SH 115</u>, Penrose, CO 81240
- 3. Have the mineral interests been severed from the subject property? O YES O NO
 - a. If yes (severed) who is the mineral interest owner? Research shown, rights have not been severed
- 4. Is the property currently developed? YES O NO
- 5. Existing types & sizes of structures: (1) Metal Sided Garage 912sf (2) Conn-ex 40'X8'
- 6. Proposed types & sizes of structures: (3) Commercial Industrial PEMB's total 17,970sf
- 7. Lot Coverage (indicate percent or square footage): Existing <u>2%</u> Proposed <u>28%</u>
- 8. FCZR Citing <u>4.14.2.30</u> Property size (acres or square footage) <u>59,183sf</u>
- 9. Amount of the property the use will encumber: <u>84.4%</u>
- 10. Zone District: B-Business Land Use Storage Facility
- 11. Please indicate the zone district & current land use for adjoining properties:
 - a. Northerly: (ZD) <u>B-BUSINESS</u> Land Use: <u>SINGLE-FAMILY RESIDENTIAL</u>
 - b. Easterly: (ZD) AR-AGRICULTURAL RURAL Land Use: UNDEVELOPED
 - c. Westerly: (ZD) AL-AGRICULTURAL LIVING Land Use: UNDEVELOPED
 - d. Southerly: (ZD) AR-AGRICULTURAL RURAL Land Use: AUTOMOTIVE/TRUCKING COMPANY
- Master Plan Planning District of property: <u>PENROSE/BEAVER PARK PLANNING DISTRICT</u> (please refer to Chapter four and planning district of the Fremont County Master Plan)
- 13. Name(s) and type(s) of road(s) the property is accessed from:

COLORADO STATE HIGHWAY 115 FUTURE: Access to Future "H" Street

14. Is access through adjacent properties? O YES O NO If yes, is access legally established through:

□ Deed of record □ Recorded Plat □ Court Order (Documentation shall be provided)

- 15. Estimated Traffic Count <u>36</u> (per day) Number of access points (1) Proposed (1) Future

- 18. Does the property lie within the boundaries or within ¼ of a mile of any service district?

☑ YES □ NO Entity Name(s) PENROSE WATER DISTRICT, FLORENCE FIRE PROTECTION DISTRICT

19. Requested duration of proposed use: _____ Ife of use 🛛 Estimated life of use vears

20. Is temporary cessation proposed: **O** YES **O** NO Duration: _____

- 21. Is buffering required: **O** YES **O** NO (Contractor yards, Junk yards, Automobile graveyards, & Vehicle impoundment yards **require** buffering per FCZR 5.17.15)
- 22. Is landscaping proposed: **O** YES **O** NO a waiver is requested
- 23. Total parking spaces <u>0</u> standard size <u>0</u> compact <u>0</u> ADA <u>0</u> (Standard 9' X 18') (Compact 7' X 15') (Please refer to section 5.3 & 5.4 of the FCZR)
- 24. Will the parking area include lighting? **O** YES **O** NO

25. Parking area surface type: <u>None</u> Thickness: <u>None</u>

- 26. Is a loading/unloading area proposed? YES NO Size: CONCRETE ____ Thickness: 6 Inches
- 27. Will hazardous materials be stored on site? O YES O NO
- 28. Will noxious weed control measures be included in the scope of the project? YES NO
- 29. Will any equipment meeting the Colorado Revised Statute definition of Special Mobile Machinery be stored or used onsite? YES NO
- 30. Mark all services and facilities necessary to accommodate the proposed use in addition to Fire Protection, Emergency Medical Response, & Law Enforcement: N/A

□ Roadway Maintenance □ Hospital □ Park & Recreation

| 🗆 Airport | 🗆 Search & Rescue | Schools | 🗆 Librar |
|-----------|-------------------|------------|----------|
| L Airport | L Search & Rescue | LI Schools | ∐ Libr |

- 31. Utility Provider information: Please provide the name of provider below:
 - a) Water: PENROSE WATER DISTRICT
 - b) Sanitation: <u>N/A</u>
 - c) Electrical: Black Hills Energy
 - d) Telephone: <u>TBD Cellular</u>
 - e) Refuse: <u>N/A</u>______
 - f) Irrigation Water: _____
 - g) Natural Gas/Propane: <u>Black Hills Energy</u>
 - h) Cable Television: <u>TBD</u>

Impact Analysis (Section 2)

 Dust and erosion control measures:
 <u>All areas will be stabilized with buildings, pavement, or vegetation to minimize erosion and the generation of fugitive dust</u> after completion of the project. During construction, industry standard erosion and dust control BMP's, such as vehicle tracking, silt fence, watering access areas, will be implemented

Noise control measures: Noise impact anticipated during construction is associated to typical construction activity

Post construction - no impact is anticipated

3. Odor control measures: Odor impact anticipated during construction is associated to typical construction activity

Post construction - no impact is anticipated

4. Visual impact control measures: <u>Visual impact anticipated during construction is associated to typical construction activity</u>

Post construction-native vegetation shall be utilized to enhance the visual corridor of HWY 115

- 5. Wildlife/plant habitat protection measures: Per species list provided, protection measures N/A
- Water quality and/or water way(s) protection measures: <u>EXTENDED DETENTION BASIN - please reference Drainage Report emailed 3/26/2024.</u>
- Safety measures to protect adjacent properties, residents, & agricultural operations: An extended detention basin is proposed to reduce the 100-year discharge from the developed site and is not

anticipated to adversely impact neighboring properties or downstream drainage conditions. In regards to the irrigation;

the site is graded away from the Brush Hollow Supply Ditch to prevent runoff from entering the ditch.

 Measures to protect and/or preserve archaeologically or historically significant sites: Per a conversation with the Owner, no discovery of any historical or archaeological significance has ever been made on

site, nor any artifacts of such significance ever been located on this property.

 Measures to limit or control offsite discernable vibrations: Little to no vibrations are anticipated during or post construction of this project.

Required Submittals Attachments (Section 3)

- 1. Current Deed of Record
- Water supply documentation: Public water source requires documentation evidencing ability to provide service. Wells require documentation of a well permit and/or documentation that the existing well is adequate for the proposed use
- 3. Fremont County's Colorado Division of Water Resources Information Form
- 4. Sanitation Documentation: Public sewer shall require documentation evidencing ability to provide service. Onsite Waste Water System (OWTS) shall require a percolation test and report and a design plan from a certified engineer. Existing OWTS systems shall require documentation that the existing system is adequate for the proposed use
- Refuse Plan: Shall address the storage, collection, and disposal of refuse. It shall also document screening of refuse receptacles/areas. (Refuse plans require approval by the Fremont County Environmental Health Dept.)
- 6. Drainage Plan: Must contain all required items under FCZR 5.10 (Drainage plans require approval by the County Engineer).
- 7. Landscaping Plan or justification for waiver request.
- 8. Lighting Plan or justification for waiver request
- 9. Noxious Weed Control Plan or justification for waiver request. (Plans and waiver requests require approval by the Fremont County Noxious Weed Manager)
- 10. List of owners and mailing address for all properties located within a five-hundred (500') foot radius of the subject property
- 11. County Roadway Impact Analysis Form (If accessed off a county road)
- 12. Colorado Department of Transportation Access Permit (If accessed off a CDOT controlled road)
- 13. Statement indicating how the proposed use complies with "Goals Objectives, and Implementation Strategies" of the Fremont County Master Plan District
- 14. Statement indicating how the proposed use will be in harmony and compatible with surrounding land uses and development in the area and/or measures that can be taken to make it in harmony & compatible.
- 15. Fire protection plan addressing method of fire protection, location of hydrants or other means of protection. If located within a fire protection district the plan shall be approved by the District.
- 16. A detailed utility plan showing the proposed or existing location of all utilities.
- 17. Site Plan drawn to professional standards (3 hard copies 18" x 24" or 24" x 36")
- 18. Submittals and exhibits should be clearly identified with section and/or question number located on the bottom right hand corner, or otherwise tabbed or marked.

If Applicable Submittals

- 19. CDOT Notification form of Proposed Land Use and comments (if access is from or within 500' of a CDOT controlled road)
- 20. Mineral Interest Notification and certified mailing receipt. Notification & Mailing shall be completed within 30 days prior to the scheduled Planning Commission Meeting. (this is only required if the minerals interests are severed)
- 21. Copies of all local, state and federal licenses and/or status of applications.
- 22. In circumstances of Corporate Ownership, documentation evidencing whom is eligible to execute documents on behalf of the corporation
- 23. In circumstances where the applicant is not the owner written authorization from the owner specifying the extent to which the representation is authorized
- 24. In circumstances where a consultant is making application on behalf of the owner, written authorization from the owner specifying the extent to which the representation is authorized
- 25. In circumstances where the property owner of record is not involved in the operation or application, documentation indicating right to occupy and use the property shall be provided. (lease or similar document)
- 26. Buffering Plan (If required)
- 27. Current registration for SMM equipment or documentation that equipment is on tax rolls associated with the property, to include list of machinery.
- 28. List of Hazardous materials stored and/or used on site, to include location of storage and management practices
- 29. Copies of mining and reclamation plans (CUP's)
- 30. Required information set forth in FCRZ 8.13.17.1 (Airports)
- 31. Required information set forth in FCRZ 8.13.17.2 (Adult Uses)
- 32: Required information set forth in FCRZ 8.13.17.3 (Kennels)
- 33. Required information set forth in FCRZ 8.13.17.4 (Antennas & Towers)

Site Plan Drawing Requirements

- a. Drawing Size: Minimum sheet size 18" x 24" to a maximum sheet size of 24" x 36";
- b. Written and graphic scale with minimum of 1" = 200' max 1" = 50';
- Appropriate title (SPECIAL REVIEW USE PERMIT, CONDITIONAL USE PERMIT, COMMERICAL DEVELOPMENT PLAN FOR {name};
- d. Appropriate subtitle (brief description of the proposed use);
- e. Boundary drawing of the property with bearings and dimensions illustrating the legal description;
- f. Legal description of the property;
- g. Acreage or square footage of the subject property;
- Lassification of the subject property;
- i. Zoning classification of the adjoining properties;
- j. North Arrow;
- k. Vicinity map locating the subject property in relation to surrounding areas;
- I. Table indicating relationship between proposed and existing construction to remain on the property
- m. Minimum lot size, maximum lot coverage, maximum building height, minimum lot width, minimum setback requirements (Front, Two sides, & Rear)
- n. Size and shape of all existing & proposed structures: each structure shall be labeled/noted as existing or proposed. Dimensions from at least two property lines shall be noted;
- o. Location of all parking areas to include size, dimensions, surface type & thickness, type of space (ADA, Standard, Compact) and a table specifying the minimum numbers of spaces required for each category;
- p. Location of loading areas to include size, dimensions surface type & thickness;
- Labeled access points including interior roadways with dimensions, surface type & thickness, circulation pattern, and dimensions from property lines;
- r. Any proposed pedestrian areas & walkways to include dimensions, surface type & thickness;
- s. Location and dimensions of refuse areas;
- t. Identification and location of all drainageway, drainage facilities, including FEMA flood areas, to include dimensions from property lines;
- u. Location, height & type of lighting for parking and off-loading areas;
- Location, type, and size of all on-site identification signage (table may be used);
- w. All easements (existing & proposed) to include dimensions from property lines (beginning, end, & centerline) width, and if they are to be vacated or relocated;
- x. Significant natural features;
- y. Soil types
- z. Open space areas
- aa. Legend identifying symbols and/or lines

By signing this Application, the Applicant, or the agent / representative / consultant acting with due authorization on behalf of the Applicant, hereby certifies that all information contained in the application and any attachments to the Application, is true and correct to the best of the Applicant's knowledge and belief.

The Applicant understands that required private or public improvements imposed as a contingency of approval for the application may be required as a part of the approval process.

Fremont County hereby advises the Applicant that if any material information contained herein is determined to be misleading, inaccurate or false, the Board of County Commissioners may take any and all reasonable and appropriate steps to declare null and void, any actions of the Board regarding the Application.

Signing this Application is a declaration by the applicant that all plans, drawings and commitments submitted with or contained within this Application are or will be in conformance with the requirements of the Fremont County Zoning Resolution.

| Anna Fluckey | | Anna Fluckey E=anha.fluckey@mccauleyconstructors.com, CN=Anna Fluckey Date: 2024.02.27 15:45:58-07'00' | Applicant |
|--------------|---------------------|--|-----------|
| Printed Name | Applicant Signature | Date | |
| John Edgar | | Please see attached Owner Authorization | Owner |
| Printed Name | Owner Signature | Date | |



FREMONT COUNTY'S COLORADO DIVISION OF WATER RESOURCES INFORMATION FORM FOR SPECIAL USE, ZONING, AND OTHER LAND USE ACTIONS

The Fremont County Department of Planning & Zoning (Department) is required to submit proposed land use actions to the State Engineer's Office (SEO) at the Colorado Division of Water Resources (CDWR). The SEO is responsible for providing an opinion regarding material injury likely to occur to decreed water rights by virtue of diversion of water necessary or proposed to be used to supply the proposed land use action.

This CDWR Information Form must be filled out completely and accurately to ensure that the submittal to the CDWR regarding this proposed land use action includes the necessary information required by that agency. The CDWR has 21 days to respond to County submittals. Incomplete submittals will be returned to the County for additional information and then must be resubmitted to the CDWR.

Please note that the CDWR timeframe for review may not coincide with the County deadlines or meetings, and if the CDWR requires additional information, further delays may occur.

Attachments can be made to this application to provide expanded narrative for any application item including supportive documentation or evidence for provided application item answers. Please indicate at the application item that there is an attachment and label it as an exhibit with the application item number, a period and the number of the attachment for that item (as an example, the first attached document providing evidence in support of the answer given at application item number 8 would be marked - Exhibit CDWR-8.1, the fifth attached document supporting the narrative provided for application item 8 would be marked - Exhibit CDWR-8.5). Exhibit numbers should be placed in the lower right hand area of the exhibit.

- 1. Name of proposed project: Penrose RV & Boat Storage
- 2. Provide a map of proposed improvements with an identified location that includes a quarterquarter, section, township, range and principle meridian (PLSS).
- A PARCEL OF LAND LOCATED WITHIN A PORTION OF THE NW 1/4 OF SECTION 28, TOWNSHIP 18 SOUTH, RANGE 68 WEST OF THE SIXTH PRINCIPAL MERIDIAN, COUNTY OF FREMONT, STATE OF COLORADO, BEING MORE PARTICULARLY DESCRIBED AS FOLLOWS: LOT 2, COYLE-VANEGMOND LOT LINE ADJUSTMENT, ACCORDING TO THE RECORDE PLAT THEREOF, FILED FOR RECORD ON JANUARY 23, 1996 IN BOOK 1237 PAGE 531. AS RECEPTION NO. 642721 IN THE RECORDS OF THE PUEBLO COUNTY CLERK AND RECORDER, COUNTY OF PUEBLO, STATE OF COLORADO.
 4. What is the size of the existing parcel? <u>59,183</u> Acres --- X Square feet
 5. What are the proposed uses of the subject property? Residential Only X Commercial Commercial and Residential
 6. What are the current uses of water on this parcel? Domestic
 - a. Are there any established uses that require water? \Box Yes --- \boxtimes No
 - b. Number of existing homes: No existing home, but has a comm/res water designation for this development

| | | If one or more, date this use was established: 2019 |
|----|----|--|
| | c. | Home lawn / garden irrigation: 🗌 Yes 🔀 No |
| | | If yes, amount: Acres Square feet |
| | | Date this use was established: |
| | d. | Livestock watering: 🗌 Yes 🔀 No |
| | | If yes, commercial or non-commercial livestock? (Circle one) |
| | | If yes, date this use was established: |
| | e. | Other uses: |
| | | Dates established: |
| 7. | W | hat will be the proposed uses of water for this parcel? Domestic |
| | a. | Number of proposed homes (including the home above if it will remain): |
| | b. | Lawn / garden watering, amount: Acres Square feet |
| | c. | Livestock watering: 🗌 Yes 🔀 No |
| | | If yes, commercial or non-commercial livestock? (Circle one) |
| | d. | Number of Employees per day: _0 Number of days open per year: _365 |
| | e. | Number of Customers per day: 13 Number of days open per year: Site is self-serve, so approx. 365 |
| | f. | Bed / Breakfast Customers per day: <u>N/A</u> Number of days open per year: <u>N/A</u> |
| | g. | Describe other water needs: _ TBD - This site is under consideration for a |
| | | landscape waiver request as well as a BOZA |
| | | Variance for a reduced set-back, which will |
| | | drastically reduce the amount of landscaped area. |
| 8. | So | urce of water for the uses described above: (If more than one source is utilized for parcel, |
| 0. | | scribe which sources will supply which proposed uses) Private: Penrose Water District |
| | - | |
| | a. | Is Municipal water available to parcel: Yes X No |
| | b. | Is water available to parcel from an independent water district? Yes X No |
| | c. | Are the uses described above proposed to be provided water by a municipality? |
| | | Yes X No |
| | | Name of provider: _Penrose Water District |

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d. Is water hauled: Yes --- X No

| e. | Is there an existing permitted well?: | Yes 🗙 No |
|----|---------------------------------------|----------|
| | If yes, permit number: | |

f. Is there a Substitute Water Supply Plan? (Substitute water supply plans provide water users a mechanism to replace out-of-priority depletions on an interim basis.)
Yes --- X No

| If yes, | name | of pl | lan: |
|---------|------|-------|------|
| | | | |

- g. Is there an unregistered well? Yes --- X No
- h. Is there a Surface Spring? 🗌 Yes --- 🗶 No

If yes, Court Adjudication Number and Spring Name:

- 9. What is the Waste Water Method?
 - ____ Municipal
 - X Septic with Leach Field
 - Closed Vault, Waste Water hauled to:

By signing this form, the Applicant, or the agent/representative acting with due authorization on behalf of the Applicant, hereby certifies that all information contained in the form and any attachments to the form, is true and correct to the best of Applicant's knowledge and belief.

Fremont County hereby advises Applicant that if any material information contained herein is determined to be misleading, inaccurate or false, the Board of Commissioners may take any and all reasonable and appropriate steps to declare actions of the Department regarding the Application to be null and void.

Signing this form is a declaration by the Applicant to conform to all plans, drawings, and commitments submitted with or contained within this form, provided that the same is in conformance with the Fremont County Zoning Resolution.

| Anna Fluckey | Anna Flucke | Digitally signed by Anna Fluckey DN: C=US, E=anna.fluckey@mccauleyconstructors.com, CN=Anna Fluckey Date: 2024.02.20 08:38:13-07'00' |
|--|-----------------------------|--|
| Applicant Printed Name | Signature | Date |
| John Edgar | _,Please see attached Lette | r of Authorization |
| Property Owner Printed Name (If different from applicant) | Signature | Date |



May 20, 2024

Fremont County Department of Planning and Zoning 615 Macon Avenue, Room 210 Canon City, CO 81212

Re: Penrose RV & Boat Storage, 17225 SH 115, Penrose, CO

To whom it may concern:

For your consideration, is the above-referenced project, outlined below. Thank you in advance.

Introduction:

The Penrose RV & Boat Storage project envisions the transformation of Lot 2 within the Coyle-Vanegmond Lot Line Adjustment Subdivision into a modern and efficient storage RV facility. Situated on a 1.36-acre site zoned B – Business Zone District, this development aligns with the County's vision for "uniform, steady growth." The primary goal is to not only contribute significantly to the economic development of Fremont County but also to ensure harmony with the historic and scenic attributes of the territory.

Preservation of Natural Landscape:

The natural landscape within and surrounding the project site is unique to the Penrose region, setting it apart from the diverse plant communities prevalent throughout Colorado. In adherence to a preservation-oriented approach, the landscape design will endeavor to respect the integrity of the existing natural surroundings, integrating indigenous plant materials. The ultimate design of the landscape plan will contemplate the incorporation of native plant specimens that not only enhance ecological authenticity but also demonstrate a conscientious approach to water conservation. Additionally, our design will strive to enhance the visual corridor along highway 115. The proposed site layout and building configuration are planned to minimize impacts to neighboring property owner's views and frame views with enhanced landscape screening of the natural landscape.

Compatibility with Neighboring Uses:

Acknowledging the importance of community integration, the Penrose RV & Boat Storage project is designed with a keen understanding of the existing land uses in the vicinity. Neighboring businesses, such as WD Trucking and Silverline Trailers, have impacted our design decisions, ensuring architectural site design with the local economic ecosystem in mind. This compatibility enhances the overall functionality and acceptance of the storage facility within the community. The facility will be screened and secured using wrought iron fencing and gates.



Collaborative Services and Development:

In an effort to enrich the surrounding area, the Penrose project extends its services in collaboration with neighboring businesses and developments. Notably, the integration of services aligns with the establishment of a new Recreational Vehicle Park in the area. The project contributes not only to its own success but also to the broader enhancement of the local recreational vehicle storage and economic landscape.

Strategic Accessibility:

Accessibility is paramount to the success of the Penrose RV & Boat Storage project. A planned new entry from Hwy 115, currently under review for CDOT approval, ensures ease of access for both clients and service providers. This access point not only enhances the project's functionality but also mitigates potential traffic concerns, demonstrating our commitment to responsible, safe and efficient development.

Sustainable Infrastructure:

The Penrose project recognizes the importance of responsible resource utilization. Existing water services, tapped and accessible at the project site, are integrated into the development. These services are currently invoiced to the property owner on a regular billing cycle. The project will be designed to meet all local building and energy compliance codes.

Lighting and Photometric Design:

Our commitment to creating a secure and inviting environment extends to the realm of lighting and photometric design. Thoughtful placement of lighting fixtures, adhering to industry best practices, ensures both safety and aesthetic appeal throughout the storage facility. The design incorporates energy-efficient (LED) lighting solutions that not only minimize environmental impact but also contribute to operational cost-effectiveness. A comprehensive photometric analysis will be conducted to optimize light distribution, preventing glare and shadows while enhancing visibility and safety for the clients and staff during all hours of operation.

Fire Protection:

A new hydrant is proposed near the site entrance, as there are no other hydrants near-by. This new proposed hydrant shall be the provided method of fire protection.

Refuse Disposal:

No on-site refuse disposal services shall be provided.

Conclusion:

In conclusion, the Penrose RV & Boat Storage project will offer a needed amenity to the area; it is a harmonious integration of thoughtful design, community collaboration, and advanced lighting solutions, by addressing the economic needs of Fremont County and respecting the historical and scenic qualities of the area.

TECHNICAL MEMORANDUM

TO: Penrose Water District

FROM: Civil Resources, LLC

DATE: May 20, 2024

RE: Penrose RV & Boat Storage 17225 SH 115 Water Demand Memo

This memorandum discusses the estimated domestic and irrigation water use for the proposed Penrose RV & Boat Storage project located 17225 SH 115. The project includes the construction of three (3) indoor storage garages. A secure hose bibb will be provided for property maintenance use. The hose bibb will not be available for filling RVs or other tenant use.

The Penrose Water District (District) currently serves this Site with a 3/4 x 5/8 domestic service. Per District policy, the maximum allowable usage for this service is:

- 10 gpm Peak Flow
- 1 3 gpm Continuous Flow
- 4,400 Maximum Gallons Per Day
- 134,200 Maximum Gallons Per Month

ESTIMATED DOMESTIC USAGE

The estimated hose bibb usage assumes that the caretaker uses a pressure washer at 3 GPM to clean out one storage unit per week at tenant turnover. The actual turnover is expected to be much less than 1 per week, as typically these units lease on a yearly basis. Based on these conservative assumptions, the projected daily water use is 4 GPD, and 124 Gallons per Month.

| | Total | |
|------------------|-----------|--|
| | (GALLONS) | Notes |
| Locked Hose Bibb | 4 | Assumes washing 1 bay per week; 3 GPM x 10 minutes, divided by 7 |
| | 4 | Total Average Day |
| | 124 | Total Average Month |

TABLE 1: SUMMARY OF EXPECTED USE

Penrose Boat & RV Storage – Water Demand Memo Prepared: May 20, 2024 Page 2 of 2

CIVIL RESOURCES STRONG DESIGN. ENDURING VALUE.

CONCLUSION

The estimated and allowable water usage is compared below:

TABLE 2: ESTIMATED VS ALLOWABLE USEAGE

| | Estimated | Allowed |
|------------------------------|-----------|---------|
| Peak Flow (GPM) | 3 | 10 |
| Maximum Daily Use (Gallons) | 4 | 4,400 |
| Maximum Monthy Use (Gallons) | 124 | 134,200 |

Overall, the Site has a projected water demand within the allowable parameters for the existing service.

Prepared by: Jim Brzostowicz, P.E. Reviewed by: Rebekah Janquart, E.I.

Attachments: Excerpt from Resolution 19 AWWA M22

J:/McCauley Construction 355\355.001.02 Penrose RV Storage/Memos & Reports\Water\Penrose RV Water Use Memo.docx





CIVIL

RES **→**URCES, LLC

DRAINAGE REPORT For PENROSE RV & BOAT STORAGE

COUNTY OF FREMONT STATE OF COLORADO

PREPARED FOR:

McCauley Constructors 605 Innovation Cir. PO Box 200 Windsor, CO 80550

PREPARED BY:

Civil Resources, LLC 8308 Colorado Blvd. Suite 200 Firestone, Colorado 80504

PREPARED: FEBRUARY 2024

REVISED: MAY 2024

Drainage Report

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3

ENGINEER'S CERTIFICATION OF DRAINAGE REPORT

"I hereby certify that this report for the preliminary drainage design of Penrose RV & Boat Storage was prepared by me (or under my direct supervision) in accordance with the provisions of the Urban Drainage Flood Control District Storm Drainage Criteria and supplemental Fremont County requirements for the owners thereof."

Jim Brzostowicz Registered Professional Engineer State of Colorado No. 40551



1.0 BACKGROUND

1.1 Location

The Penrose RV & Boat Storage project is located at 17225 Highway 115, situated in the northwest one-quarter of Section 28, Township 18 South, Range 68 West of the 6th Principal Meridian, County of Fremont, State of Colorado. The Site includes Lot 2 of the Coyle-Vanegmond lot line adjustment, and is surrounded by Colorado State Highway 115 (SH 115) to the southeast, the Brush Hollow Supply Ditch to the north, and undeveloped land to the west. The lot is currently zoned B – business, per the Fremont County Zoning Resolution. Refer to Figure 1 for a project vicinity map.



Figure 1: Project Vicinity Map

1.2 Description of Property

The Penrose RV & Boat Storage project proposes to develop the existing Lot 2 of the Coyle-Vanegmond lot line adjustment into approximately 25 storage units for boats and recreational vehicles. The lot contains 1.36 acres of mostly undeveloped land, with an existing garage and shipping container unit. The total drainage area analyzed for the purposes of this drainage report is 2.44 acres, which includes some off-site areas which contribute runoff to the Site.

The Site generally slopes to the southwest with an average grade of 6%. On-site soils can be classified as Hydrologic Soil Group B, per the Natural Resources Conservation Service (NRCS) web soil survey. The Site lies within Zone X, area of minimal hazard, per FEMA National Flood Hazard Layer. Refer to Appendix A for a soils map and FIRMette.

2.0 DRAINAGE BASINS

2.1 <u>Historic Drainage Basins</u>

The existing Site can be divided into three (3) on-site historic drainage basins, and four (4) off-site basins. The existing overall impervious coverage is 10.1%. Refer to Appendix B for historic runoff calculations.

- Basin H-1 is located along the west property line and contains 0.12 acres of undeveloped land. Runoff in this
 basin generally flows south from the undeveloped area to the existing roadside swale along SH 115, and
 continues southwest, off-site. The impervious coverage of Basin H-1 is 2.0% and the 100-year historic runoff
 coefficient is 0.44.
- Basin H-2 contains 1.03 acres of the central portion of the Site, including two existing buildings and landscaped area. Runoff generated in this basin sheet flows south from the central portion of the Site to Basin HOS-2, where it then flows southwest. The impervious coverage of this basin is 8.4% and the 100year historic runoff coefficient is 0.46.
- Basin H-3 contains the east portion of the Site, and consists of 0.20 acres of undeveloped land. Runoff in this basin sheet flows south to the roadside swale. Runoff is conveyed southwest via an 18-inch corrugated metal pipe culvert, into Basin HOS-3. The impervious coverage of the basin is 2.0% and the 100-year historic runoff coefficient is 0.44.
- Basin HO-1 is located west of Basin H-1 on the west property line, and contains 0.06 acres of undeveloped land. Runoff in this basin sheet flows east into basin H-1. The impervious coverage of this basin is 2.0% and the 100-year historic runoff coefficient is 0.44.
- Basin HOS-1 is located southeast of Basin H-3 between the property line and SH 115. This basin contains 0.41 acres of landscape area and an existing roadside swale. Runoff in the basin sheet flows to the roadside swale and flows southwest via an 18-inch corrugated metal pipe culvert. The impervious coverage of this basin is 15.2% and the 100-year historic runoff coefficient is 0.50.
- Basin HOS-2 is located south of Basin H-2, and contains landscape area and the roadside swale. Runoff sheet flows to the swale, where it channelizes and flows southwest. The impervious coverage of this basin is 15.2% and the 100-year historic runoff coefficient is 0.50.
- Basin HOS-3 is located west of the Site along the property line, and contains 0.12 acres of undeveloped land. Runoff in this basin sheet flows west, off-site. The impervious coverage of this basin is 13.4 cfs, and the 1000-year historic runoff coefficient is 0.44.

2.2 Proposed Drainage Basins

Under developed conditions, the Site can be divided into ten (10) on-site drainage basins and four (4) off-site basins. On-site basins tributary to the detention pond are denoted "S", while off-site basins tributary to the pond are denoted "O". On-site basins bypassing detention are denoted "SO", while off-site basins bypassing detention are denoted "OS". The overall impervious coverage of the developed Site is 31.0%. The Site has not been studied as part of a Master Drainage Report.

 Basin S-1 is located along the north and west property lines. The 0.21-acre basin contains a conveyance swale and landscape area. Runoff in this basin sheet flows to the conveyance swale, where the runoff channelizes and flows west and south to the detention pond. The impervious coverage of this basin is 2.7% and the 100-year developed runoff coefficient is 0.44.

- Basin S-2 is 0.07 acres and contains the roof area of Building B. Runoff developed in this basin will be collected in roof leaders, and surface discharge via downspout to the swale in Basin S-1. The impervious coverage of the basin is 90% and the 100-year developed runoff coefficient is 0.84.
- Basin S-3 is 0.14 acres and contains the roof area of Building A. Runoff in this basin will be collected in roof leaders, and surface discharge via downspout to the swale in Basin S-1. The impervious coverage of this basin is 90% and the 100-year developed runoff coefficient is 0.84.
- Basin S-4 is located in the center of Lot 2, and contains 0.48 acres of the proposed drive aisles. Runoff in
 this basin sheet flows to a swale centered in the drive aisle, where the runoff channelizes and flows west
 and south. The swale terminates at the edge of the drive aisle, and runoff enters a second swale, adjacent
 to the property line, via a riprap rundown. From there, the runoff flows southwest to the detention pond in
 basin PND. The impervious coverage of the basin is 38.3% and the 100-year developed runoff coefficient
 is 0.60.
- Basin S-5 is 0.20 acres and contains the roof area of Building C. Runoff generated in this basin will be collected in roof leaders and conveyed to the property line swale in Basin S-4 via an 8" PVC header pipe. The impervious coverage of this basin is 90% and the 100-year developed runoff coefficient is 0.84.
- Basin PND is located in the southwest corner of the Site and contains the 0.08-acre detention pond. Runoff
 generated in this basin will be captured by the detention pond outlet structure and discharge to the existing
 roadside swale, via a 12" outfall pipe. The impervious coverage of this basin is 4.1% and the 100-year
 developed runoff coefficient is 0.45.
- Basin O-1 is an off-site basin, located along the west property line. This basin contains 0.06 acres of
 undeveloped landscape area, with an impervious coverage of 2.0% and a 100-year developed runoff
 coefficient of 0.44. Runoff in this basin sheet flows east to the conveyance swale in Basin S-1, and is
 ultimately detained in the pond.
- Basin OS-1 is an off-site basin, located in the SH 115 right-of-way, between the southeast property line and the highway. The basin contains 0.51 acres of landscaped area and a roadside swale. Runoff in this basin sheet flows to the swale, where it channelizes and flows southwest to an 18-inch culvert under the proposed access drive. The impervious coverage of this basin is 15.6% and the 100-year developed runoff coefficient is 0.50.
- Basin OS-2 is an off-site basin located in the SH 115 right-of-way, between the detention pond and the highway. This basin is 0.40 acres and contains the proposed access drive, the roadside swale, and landscaped area. Runoff generated in this basin sheet flows to the swale, where it channelizes and flows southwest to an existing 18-inch corrugated metal pipe culvert. This basin receives the outflow from the detention pond. The impervious coverage of this basin is 22.8% and the 100-year developed runoff coefficient is 0.53.
- Basin OS-3 is an off-site basin, located at the southwest corner of the Site, which contains 0.11 acres of landscaped area. Runoff in this basin generally sheet flows south to the roadside swale. The impervious coverage of this basin is 14.9% and the 100-year developed runoff coefficient is 0.50.
- Basin SO-1 is an on-site basin, located at the eastern corner of the Site. The basin contains 0.12 acres of
 landscape area with a swale. Runoff in this basin will sheet flow to the swale, then flow southeast and
 discharge into basin OS-1 without being detained. The impervious coverage of this basin is 2.0% and the

100-year developed runoff coefficient is 0.44.

- Basin SO-2 is an on-site basin, located at the driveway entrance to the Site. The basin contains 0.02 acres
 of gravel driveway surface. Runoff in this basin sheet flows south into Basin OS-2, without being detained.
 The impervious coverage of this basin is 40.0% and the 100-year runoff coefficient is 0.61.
- Basin SO-3 is an on-site basin, located at the southwest corner of the Site, between the property line and detention pond. The basin contains 0.03 acres of landscape area and the detention pond emergency spillway. Runoff in this basin will sheet flow south/southeast and discharge into basin OS-2 without being detained. The impervious coverage of this basin is 8.1% and the 100-year developed runoff coefficient is 0.46.
- Basin SO-4 is an on-site basin, located along the western property line, west of the detention pond. The basin contains 0.02 acres of landscape area. Runoff in this basin will sheet flow south and discharge into basin OS-2 without being detained. The impervious coverage of this basin is 40.0% and the 100-year developed runoff coefficient is 0.44.

3.0 DRAINAGE DESIGN CRITERIA

3.1 Regulations

The proposed drainage design complies with the regulations set forth in the Subdivision Regulations of Fremont County, last amended January 2020, as well as the Mile High Flood District's (MHFD) Urban Storm Drainage Criteria Manual, version prior to March 2024 updates (USDCM).

3.2 <u>Development Criteria Reference and Constraints</u>

The Subdivision Regulations state that the peak runoff for the developed Site must not exceed the historic peak runoff for the same storm event. Furthermore, stormwater detention facilities shall not release runoff at a rate higher than the historic runoff rate. The proposed development of the Site will increase the overall runoff as a result of increase impervious area. To adhere to the regulations set forth by the Fremont Couty, a detention pond will be used to temporarily store developed runoff and discharge at a rate less than or equal to the historic rate.

3.3 Hydrological Criteria

The hydrology of the Site was determined using the methods described in the Subdivision Regulations of Fremont County, last amended January 2020, as well as the Mile High Flood District's (MHFD) Urban Storm Drainage Criteria Manual, latest version (USDCM). The following methods were utilized:

- The Rational Method was utilized to estimate the 10- and 100-year peak flowrates as the minor and major storm events, respectively.
- Runoff coefficients for the Site were determined from land usage and hydrologic soil group data as outlined by Tables 6-3 through 6-5 of the USDCM.
- The design point rainfall values used in the Rational Method were obtained from NOAA Atlas 14 Precipitation Frequency Data Server, and are included in Appendix A.
- The Modified FAA Method and Colorado Urban Hydrograph Procedure were utilized to estimate the required 100-year detention volume for the Site.

3.4 Hydraulic Criteria

- The detention pond outlet structure was designed using the MHFD outlet structure workbook. The detention pond
 will utilize an outlet structure with water quality orifice plate, overflow weir, and outflow pipe with a restrictor plate
 for 100-year peak flow events or smaller, and an emergency spillway for events exceeding the 100-year storm.
- The Hydraflow Express software was used to model the proposed culverts and roof drain. Please refer to Appendix C for Hydraflow Express output files.

4.0 DRAINAGE FACILITY DESIGN

4.1 General Concept

The proposed stormwater design will generally maintain the historic drainage patterns of the Site. The majority of developed runoff from the Site will be directed southwest toward the proposed detention pond, via sheet flow and conveyance swales. The pond will provide water quality treatment to the developed flow, and will temporarily store developed runoff and discharge from the Site at a rate equal to below the historic runoff. Outflow from the detention pond will discharge to the existing roadside swale adjacent to SH 115.

Off-site basins OS-1, OS-2, and OS-3 will continue to flow off-site, under developed conditions, and on-site basins SO-1 through SO-4 will discharge off-site without being detained. To account for this developed runoff bypassing detention, runoff tributary to the detention pond will be "over-detained". The sum of all developed runoff from basins bypassing detention and the discharge from the detention pond will be equal to or less than the historic runoff for the Site.

4.2 Specific Details

Historically, the Site discharges to the roadside swale along SH 115, and flows southwest along the highway, eventually discharging to Bear Creek. The Site is bounded by the Brush Hollow Supply Ditch on the upstream side, which may intercept upstream runoff during the minor, 10-year storm event. Upstream runoff from the major, 100-year storm will enter and flow through the Site, bypassing detention. The proposed drainage system is designed to maintain the historic drainage patterns and overall discharge point of the Site.

Developed runoff in Basin S-1 will sheet flow to a swale along the north and west property lines. The swale is designed to convey the 100-year developed runoff to the detention pond, via a type VL riprap rundown at design point S-1. The swale in Basin S-1 will also collect runoff generated from the roof areas of Building A in Basin S-3, as well as runoff from off-site, undeveloped Basin O-1. The runoff from the building will be collected in roof leaders, and surface drain, via downspouts, to the swale.

The grading in Basin S-4 is designed to capture developed runoff in a swale, centered in the gravel drive aisle, and direct the runoff south and west, where the swale terminates at a type VL riprap rundown and enters a second swale located between the property line and edge of the gravel drive. The drive aisle swale will also capture developed runoff from the roof of Building B in Basin S-2. Runoff from Basin S-5 is will be captured in roof leaders, and piped to the property line swale in Basin S-4 via an 8" PVC pipe, ultimately discharging to the detention pond

On-site Basins SO-1 through SO-4 will discharge directly off-site, bypassing the detention pond. Due to the existing grades along the property boundary easement, it is impracticable to capture runoff from these basins and direct it to the detention pond.

Off-site Basins OS-1 and OS-2 will be modified slightly from existing conditions to remove the existing access drive and 18" culvert, and relocate the drive and culvert to the southwest. The roadside swale will also be realigned and re-graded to accommodate the new location of the culvert. Basin OS-3 will remain unchanged from historic conditions.

4.3 <u>Stormwater Storage Facilities</u>

The proposed detention pond is designed to treat the WQCV and to detain the 100-year storm event. The pond was sized using the Modified FAA method and the Colorado Urban Hydrograph Procedure (CUHP). The WQCV for the area tributary to the pond was calculated to be 0.020 acre-feet. The 100-year detention volume was calculated to be 0.083 acre-feet per the CUHP, and 0.078 acre-feet per the Modified FAA method; to be conservative, 0.083 acre-feet was used as the minimum 100-year detention volume. The total required detention pond volume is 0.102 acre-feet for the WQCV and 100-year detention volume.

The detention pond will accept a total of 5.60 cfs of developed runoff during the 100-year storm from basins S-1 through S-5, PND, and OS-1. The area tributary to the pond is 1.24 acres, with a composite impervious coverage of 45.0%.

The pond outlet structure will consist of a modified Type C inlet, with a water quality orifice plate, and outfall pipe with flow restrictor. The water quality orifice plate features three (3) 3/8-inch diameter orifices spaced 5.5-inches on-center, and was sized to drain 99% of the WQCV in 43 hours, which satisfies the USDCM minimum of 40 hours. The pond will also drain 97% of the 5-year volume in 63 hours, satisfying the State maximum allowable drain time of 72 hours. Outflow from the pond will discharge to the historic discharge point – the roadside swale along SH 115. The 100-year outflow from the pond will be discharged at a rate of 2.16 cfs.

The pond will have a 5-foot-wide concrete emergency spillway along the southeast side. The invert elevation of the spillway will be 5505.00-feet, 0.01 feet above the 100-year water surface elevation (WSEL) of 5504.99-feet; furthermore, the detention pond will have a top of berm elevation of 5506.00, providing more than 1.00-foot of freeboard above the 100-year WSEL. Table 1 summarizes the stage-storage of the proposed pond. The downstream side of the spillway will be armored with type VL riprap for a length of 5-feet. The spillway was sized to convey the undetained 100-year runoff to the pond, 5.60 cfs. Refer to Appendix C for spillway sizing calculations.

| Stage | Elevation | D Elevation | Area | incremental Est. Volume | Est. Availa | ble Volume | Street Strates |
|-----------|-----------|-------------|-------|-------------------------|-------------|---------------|------------------------|
| (ft) | (ft) | (ft) | (SF) | (CF) | (CF) | (ac-ft) | Note |
| s u saith | | | No. | | | No. 291 Takes | |
| 0 | 5503.00 | 0.00 | 0 | 0 | 0 | 0.000 | Outlet Structure Inver |
| 0.50 | 5503 50 | 0.50 | 353 | 88 | 88 | 0.002 | |
| 1.00 | 5504.00 | 0.50 | 1;384 | 434 | 522 | 0.012 | |
| 1.23 | 5504.23 | 0.23 | | | | | WQCV WSEL |
| 1.50 | 5504.50 | 0.50 | 2,026 | 852 | 1,375 | 0.032 | |
| 1.99 | 5504.99 | 0.49 | | | | | 100-yr WSEL |
| 2 00 | 5505.00 | 0.50 | 2,454 | 1,120 | 2,495 | 0.057 | Spillway Invert |
| 2.50 | 5505.50 | 0.50 | 3.013 | 1,367 | 3,862 | 0.089 | opinitaly involt |
| 3.00 | 5506.00 | 0.50 | 3,776 | 1,697 | 5,559 | 0.128 | Top of Berm |

Table 1: Stage-Storage Summary

4.4 Runoff Summary

Table 2 illustrates the overall runoff from the developed Site, as compared to historic conditions.

| Point of Discharge | | Ex | Runof disting (C | | | Runoff Proposed (CFS) | | | | Total Site Discharge Proposed (CFS) | | | ∆ In Discharge from Discharge Point Proposed LESS Existing (CFS) | | | | | | | |
|-----------------------|--------|--------|---------------------|---------|----------|--------------------------|--------|--------|---------|--|----------------|----------|--|----------|--------|-------------|-------------|-----------|--|--|
| | Basin | 2-Year | 5-Year | 10-Year | 100-Year | Basin | 2-Year | 5-Year | 10-Year | 100-Year | 2-Year | 5-Year | 10-Year | 100-Year | 2-Year | 5-Year | 10-Year | 100-Year | | |
| | H-1 | 0.00 | 0.00 | 0.04 | 0.44 | S-1 | 0.01 | 0.01 | 0.05 | 0.53 | a allow the st | 11 4 210 | Courses and | | | Contractory | ACCOUNTS OF | and south | | |
| | 141 | 0.00 | 0.00 | 0_04 | 0,44 | S-2 | 0,14 | 0.18 | 0.23 | 0,45 | | | 1030 | 217 | | 100 | 163 | 12 | | |
| | H-2 | 0-14 | 0.20 | 0.57 | 3.87 | S-3 | 0,29 | 0_38 | 0.48 | 0.94 | | 10 | | 140 | nik z | 1.16.14 | | | | |
| Detention | 172 | 0.14 | 0.20 | 0.57 | 3.07 | S-4 | 0.28 | 0_40 | 0,59 | 1,79 | | | - | | | - | 198 | | | |
| Pond | H-2 | 0_01 | 0.01 | 0,06 | 0,73 | S-5 | 0,42 | 0,56 | 0,70 | 1.38 | 0.012 | 0.013 | 0.260 | 2.16 | -0.14 | -0.21 | -0.43 | -3.12 | | |
| | HO-1 | 0.00 | 0.00 0.0: | 0.02 | 0.23 | PND | 0.01 | 0.01 | 0.03 | 0.29 | | | 14 m | 1.7 | | | | | | |
| | 110-1 | 0.00 | 0.00 | 0.02 | 0,23 | 0-1 | 0.00 | 0,00 | 0.02 | 0.23 | | E. | 77.1 | | | | | | | |
| | Tolal | 0_15 | 0_22 | 0.69 | 5.28 | Total | 1.13 | 1.54 | 2 11 | 5.60 | | | | | 1 | | | 1.1 | | |
| | HOS-1 | 0.08 | 0.13 | 0.26 | 1.29 | OS-1 | 0,10 | 0,15 | 0.30 | 1.49 | | | | | 2.4 | | | | | |
| | | 0.00 | 0.10 | 0120 | 1.23 | OS-2 | 0,17 | 0.25 | 0.43 | 1.71 | | | - | | | 25.9 | | | | |
| | . 1 | | | | | OS-3 | 0.03 | 0.04 | 0.09 | 0.44 | 100 | | | | | 100 | | 1.1 | | |
| Direct Off- | HOS-2 | 0.08 | 0.13 | 0,27 | 1.34 | SO-1 | 0.00 | 0.00 | 0.04 | 0_43 | 0.31 | | 0.90 | 4.31 | | | | 1.19 | | |
| Site | | | | | | SO-2 | 0.01 | 0.02 | 0.03 | 0.08 | 0.31 | 0,47 | | 4,31 | 0.12 | 0.17 | 0.29 | | | |
| | HOS-3 | 0.03 | 0.04 | 0.09 | 0.49 | SO-3 | 0.00 | 0.01 | 0.01 | 0.10 | 81 | | 1.00 | = 2 | | | - | | | |
| 1 | 1100 0 | 0.00 | 0.04 | 0_00 | 0,43 | SO-4 | 0.00 | 0.00 | 0_01 | 0_06 | | | | 2 | | | | | | |
| | Tolal | 0.19 | 0.30 | 0.61 | 3,12 | Total | 0.31 | 0.47 | 0.90 | 4.31 | | | 1 | | | | | | | |
| Overall Site Total | | 0.34 | 0.52 | 1.31 | 8.40 | 14 | 1.44 | 2.01 | 3.00 | 9.91 | 0.32 | D.48 | 1.16 | 6.47 | -0.02 | -0.04 | -0.15 | -1.93 | | |

Table 2: Runoff Summary

Runoff from basins directly discharging off-site will increase post-development. However, the total runoff discharging from the Site will be reduced by 0.15 cfs for the minor, 10-year storm, and 1.93 cfs for the major, 100-year storm. This satisfies the criteria outlined in the Subdivision Regulations, as the peak flow discharging from the developed Site does not exceed the respective historic storm, for the 10 and 100-year events. Furthermore, the detention pond sufficiently over-detains the 10-year and 100-year runoff to account for undetained developed discharge. The total developed 10-year discharge is 1.16 cfs and 100-year discharge is 6.47 cfs. This is less than the historic 10- and 100-year discharges of 1.31 cfs and 8.40 cfs, respectively.

5.0 <u>CONCLUSIONS</u>

5.1 <u>Compliance with the Town and UDFCD Criteria</u>

This report is in compliance with the provisions outlined in the *Subdivision Regulations of Fremont County*, last amended January 2020, as well as the Mile High Flood District's (MHFD) *Urban Storm Drainage Criteria Manual*, version prior to March 2024 updates (USDCM).

5.2 Drainage Concept

The Penrose RV & Boat Storage project will improve drainage conditions in the proximity of the Site, by utilizing a detention basin. The detention basin will be used to control the discharge of runoff from the Site, by temporarily storing runoff and releasing it at a controlled rate. Runoff from the majority of the developed Site will be captured by the detention pond, and the overall developed runoff from the Site will be reduced from 8.40 cfs to 6.47 cfs, an approximate 23% reduction.

Based on these factors, the proposed project is not anticipated to have an adverse impact on the existing drainage conditions of the Site, nor its immediate vicinity.

6.0 <u>REFERENCES</u>

- Urban Storm Drainage Criteria Manual, Volumes 1, 2 and 3. Mile High Flood District. Version prior to March 2024 update.
- Subdivision Regulations od Fremont County, Colorado. Fremont County Department of Planning and Zoning. Last amended January 14, 2020.

7.0 <u>LIST OF APPENDICIES</u>

Appendix A – Figures

- Project Vicinity Map
- NRCS HSG Soils Map & Table
- FEMA FIRMette
- NOAA Atlas 14 Point Precipitation Frequency Estimates

Appendix B – Hydrologic Computations

- Developed Runoff Calculations
- Historic Runoff Calculations
- Runoff Summary

Appendix C – Hydraulic Computations

- MHFD Detention Basin Design Workbook
- MHFD Detention Volume by the Modified FAA Method
- Detention Pond Stage-Storage Table
- Hydraflow Storm Sewer Summary Report
- Emergency Spillway Analysis

Appendix D – Drawings

- Historic Drainage Plan
- Drainage Plan

APPENDIX A

Figures

ν.







Hydrologic Soil Group—Fremont County Area, Colorado

National Cooperative Soil Survey Web Soil Survey

USDA **Conservation Service** Natural Resources

Hydrologic Soil Group

| Map unit symbol | Map unit name | Rating | Acres In AOI | Percent of AOI | |
|--------------------------|--|--------|--------------|----------------|--|
| 65 | Manvel silt loam, 0 to 2 percent slopes | В | 1.5 | 100.0% | |
| Totals for Area of Inter | rest | 1.5 | 100.0% | | |

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher

National Flood Hazard Layer FIRMette





Sasemap Imagery Source: USGS National Map 2023

regulatory purposes.

unmapped and unmedernized steas cannot be used for

 \bigcirc

1,000

3,500

2,000



Precipitation Frequency Data Server

NOAA Atlas 14, Volume 8, Version 2 Location name: Penrose, Colorado, USA* Latitude: 38.4543°, Longitude: -105.014° Elevation: 5514 ft** * source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St., Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffery Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

PF_tabular | PF_graphical | Maps_&_aerials

PF tabular

| Duration | Average recurrence interval (years) | | | | | | | | | | | |
|----------|-------------------------------------|----------------------------|-----------------------------|-----------------------------|----------------------------|-----------------------------|-------------------------|----------------------------|----------------------------|----------------------------|--|--|
| | 1 | 2 | 5 | 10 | 25 | 50 | 100 | 200 | 500 | 1000 | | |
| 5-min | 0.223 (0.172-0.288) | 0.267 (0.206-0.346) | 0.349 (0.268-0.453) | 0.425 (0.325-0.555) | 0.543 (0.408-0.756) | 0.644 | 0.754 | 0.874 | 1.05 | 1.19 (0.753-1.86 | | |
| 10-min | 0.326 | 0.391 | 0.510 (0.393-0.663) | 0.622 | 0.795 | 0.943 (0.689-1.33) | 1.10 | 1.28 | 1.53 | 1.74 | | |
| 15-min | 0.398 (0.308-0.515) | 0.477 (0.369-0.618) | 0.623 (0.479-0.809) | 0.759 (0.581-0.992) | 0.969 | 1.15 (0.841-1.62) | 1.35 | 1.56 | 1.87 (1.22-2.90) | 2.12 (1.34-3.32 | | |
| 30-min | 0.565 (0.437-0.731) | 0.676 (0.522-0.875) | 0.880 (0.678-1.14) | 1.07 (0.821-1.40) | 1.37 (1.03-1.91) | 1.62 (1.19-2.29) | 1.90 (1.34-2.76) | 2.21 (1.50-3.32) | 2.65 (1.73-4.10) | 3.01 (1.90-4.70) | | |
| 60-min | 0.704 (0.545-0.911) | 0.831 (0.642-1.08) | 1.08 (0.829-1.40) | 1,32 (1.01-1.72) | 1.70 (1.28-2.38) | 2.03 (1.49-2.88) | 2.40 (1.70-3.51) | 2.82 (1.92-4.25) | 3.43 | 3.93 (2.49-6,14) | | |
| 2-hr | 0.844 (0.658-1.08) | 0.986 (0.769-1.27) | 1.27 (0.988-1.64) | 1.56 (1.20-2.02) | 2.02 (1.55-2.83) | 2.44 (1.81-3.44) | 2.91 (2.08-4.21) | 3.43 (2.36-5.13) | 4.20 (2.78-6.48) | 4.85 (3.10-7.50) | | |
| 3-hr | 0.909 (0.713-1.16) | 1.05 (0.822-1.34) | 1.34 (1.05-1.72) | 1.65 (1.28-2.12) | 2.16 (1.67-3.01) | 2.62 (1.96-3.69) | 3.15 (2.27-4.55) | 3.75 (2.60-5.58) | 4.63 (3.09-7.10) | 5.38 (3.46-8.26) | | |
| 6-hr | 1.04 (0.825-1.32) | 1.19 (0.937-1.50) | 1.50 (1.18-1.90) | 1.83 (1.44-2.34) | 2.41 (1.88-3.34) | 2.94 (2.22-4.10) | 3.54 (2.59-5.08) | 4.24 (2.97-6.26) | 5.28 (3.56-8.02) | 6.15 (4.00-9.35) | | |
| 12-hr | 1.22 (0.975-1.53) | 1.38 (1.10-1.73) | 1.73 (1.38-2.17) | 2.10 (1.66-2.65) | 2.72 (2.14-3.73) | 3.29 (2.51-4.54) | 3.95 (2.91-5.59) | 4.69 (3.32-6.85) | 5.81 (3.95-8.72) | 6.75 (4.43-10.1) | | |
| 24-hr | 1.42 (1.14-1.76) | 1.63 (1.31-2.02) | 2.04 (1.64-2.54) | 2.46 (1.96-3.08) | 3.15 (2.49-4.23) | 3.76 (2.88-5.10) | 4.45 (3.30-6.20) | 5.23 (3.73-7.51) | 6.37 (4.38-9.43) | 7.33 | | |
| 2-day | 1.63 (1.32-2.00) | 1.90 (1.54-2.33) | 2.41 (1.95-2.97) | 2.91 (2.34-3.60) | 3.69 (2.93-4.87) | 4.37 (3.37-5.83) | 5.12 (3.82-7.03) | 5.95 (4.28-8.42) | 7.16 (4.96-10.4) | 8.16 (5.47-12.0) | | |
| 3-day | 1.77 (1.45-2.16) | 2.07 (1.69-2.52) | 2.63 (2.14-3.22) | 3.17 (2.56-3.90) | 4.02 (3.21-5.27) | 4.76 (3.70-6.31) | 5.57 (4.19-7.60) | 6.47 (4.68-9.10) | 7.78 (5.42-11.3) | 8.86 (5.98-12.9) | | |
| 4-day | 1.90 (1.55-2.30) | 2.21 (1.81-2.69) | 2.81 (2.29-3.42) | 3.38 (2.74-4.14) | 4.28 (3.42-5.58) | 5.05 (3.94-6.67) | 5.91 (4.46-8.02) | 6.86 (4.98-9.59) | 8.23 (5.76-11.9) | 9.36 (6.35-13.6) | | |
| 7-day | 2.22 (1.84-2.68) | 2.59 (2.13-3.12) | 3.26 (2.68-3.94) | 3.88 (3.17-4.72) | 4.85 (3.90-6.25) | 5.68 (4.45-7.41) | 6.58 (5.00-8.83) | 7.58 (5.54-10.5) | 9.00 (6.35-12.8) | 10.2 (6.96-14.6) | | |
| 10-day | 2.50 (2.07-2.99) | 2.90 (2.40-3.47) | 3.62 (2.99-4.35) | 4.28 (3.52-5.18) | 5.29 (4.27-6.75) | 6.14 (4.83-7.94) | 7.06 (5.38-9.39) | 8.06 (5.92-11.0) | 9.48 (6.72-13.4) | 10.6 (7.32-15.2) | | |
| 20-day | 3.22 (2.70-3.82) | 3.72 (3.11-4.41) | 4.57 (3.81-5.44) | 5.32 (4.41-6.37) | 6.42 (5.20-8.03) | 7.32 (5.79-9.29) | 8.26 (6.34-10.8) | 9.25 (6.85-12.5) | 10.6 (7.60-14.8) | 11.7 (8.17-16.6) | | |
| 30-day | 3.81 (3.21-4.49) | 4.39 (3.69-5.18) | 5.37 (4.50-6.35) | 6.20 (5.17-7.38) | 7.38 (5.99-9.13) | 8.32 (6.61-10.5) | 9.28 (7.16-12.0) | 10.3 (7.64-13.7) | 11.6 (8.36-16.0) | 12.7 (8.90-17.8) | | |
| 45-day | 4.57 (3.86-5.35) | 5.27 (4.46-6.18) | 6.42 (5.41-7.55) | 7.37 (6.18-8.71) | 8.68 (7.06-10.6) | 9.68 (7.72-12.0) | 10.7 (8.27-13.7) | 11.7 (8.73-15.4) | 13.0 (9.40-17.8) | 14.1 (9.91-19.5) | | |
| 60-day | 5.22 (4.43-6.09) | 6.04 (5.12-7.05) | 7.36 (6.22-8.61) | 8.42 (7.09-9.91) | 9.85 (8.02-11.9) | 10.9 (8.73-13.5) | 12.0 (9.29-15.2) | 13.0 (9.73-17.0) | 14.3 (10.4-19.4) | 15.3 (10.9-21.2) | | |

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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PF graphical


PDS-based depth-duration-frequency (DDF) curves

| Dura | alion |
|----------|----------|
| 5-min | — 2-day |
| — 10-min | 3-day |
| — 15-min | 4-day |
| | 7-day |
| — 60-min | 10-day |
| 2-hr | - 20-day |
| — 3-hr | 30-day |
| —— 6-hr | 45-day |
| — 12-hr | - 60-day |
| —— 24-hr | |

NOAA Atlas 14, Volume 8, Version 2

Created (GMT): Tue Jul 25 22:04:26 2023

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Maps & aerials

Small scale terrain



Large scale terrain





Large scale aerial

Precipitation Frequency Data Server



Back to Top

US Department of Commerce National Oceanic and Atmospheric Administration National Weather Service National Water Center 1325 East West Highway Silver Spring, MD 20910 Questions?: HDSC.Questions@noaa.gov

Disclaimer

APPENDIX B

Hydrologic Computations



(4) (4)

¹Runoff Coefficient "C" Values are from Table 6-5 in the USDCM.

| Total | POND TOTAL | 0.7 | PND | S-5 | 5.4 | S-3 | S-2 | Ŷ. | OFF-SITE TOTAL | SO-4 | SO-3 | SO-2 | SO-1 | 0S-3 | 0S-2 | 0S-1 | 「市町町町町町町町 | いいためという | I.D. | Sub-Basin |
|---------|------------|-------|-------|-------|--------|-------|-------|-------|----------------|------|-------|------|-------|-------|--------|--------|---|----------|----------------|------------------------|
| 106,165 | 54,089 | 2,754 | 3,491 | 8,800 | 20,866 | 6,000 | 2,850 | 9,328 | 52,078 | 730 | 1,117 | 726 | 5,276 | 4,704 | 17,289 | 22,233 | Contractor | (sf) | TOTAL | |
| 2.44 | 1.24 | 0.06 | 0.08 | 0.20 | 0.48 | 0.14 | 0.07 | 0.21 | 1.20 | 0.02 | 0.03 | 0.02 | 0.12 | 0.11 | 0.40 | 0.51 | 8. 25 C | (ac) | TAL. | |
| 17,650 | 17,650 | 0 | 0 | 8,800 | 0 | 6,000 | 2,850 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | ないでは、人 | (51) | 70 | |
| 0.41 | 0.41 | 0,00 | 0.00 | 0.20 | 0.00 | 0_14 | 0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0,00 | 0.00 | 0.00 | のないのである | (ac) | Roof | |
| 8,753 | 1,920 | 0 | 0 | 0 | 1,920 | 0 | 0 | 0 | 6,833 | 0 | 52 | 0 | 0 | 537 | 3,164 | 3,079 | 10 215 | (sf) | Pav | A DATE OF |
| 0.20 | 0.04 | 0.00 | 0,00 | 0.00 | 0.04 | 0.00 | 0.00 | 0.00 | 0.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.01 | 0.07 | 0.07 | 可による | (ac) | Pavement | |
| 17,632 | 15,350 | 0 | 196 | 0 | 14,993 | 0 | 0 | 161 | 2,282 | 0 | 45 | 726 | 0 | 209 | 1,302 | 0 | 14 14 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | (sł) | G | Area |
| 0.40 | 0.35 | 0.00 | 0.00 | 0.00 | 0.34 | 0.00 | 0.00 | 0.00 | 0.05 | 0,00 | 0.00 | 0.02 | 0.00 | 0.00 | 0.03 | 0.00 | | (ac) | Gravel | S 100 |
| 62,129 | 19,168 | 2,754 | 3,294 | 0 | 3,952 | 0 | 0 | 9,167 | 42,961 | 730 | 1,020 | 0 | 5,276 | 3,958 | 12,823 | 19,153 | | (sf) | 10 | |
| 1.43 | 0.44 | 0.06 | 0.08 | 0.00 | 60.0 | 0.00 | 0.00 | 0.21 | 0.99 | 0.02 | 0.02 | 0.00 | 0.12 | 60*0 | 0.29 | 0.44 | Status Status | (ac) | LC/Open | A State |
| - | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | (51) | Hist | Nr and |
| 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0_00 | 0.00 | 0.00 | 0.00 | 0_00 | 0.00 | 0.00 | 0,00 | 0.00 | 127 | (ac) | storic | |
| 31.0 | 45.0 | 2.0 | 4_1 | 0 06 | 38.3 | 0.06 | 90,0 | 2,7 | 16.5 | 2.0 | 8,1 | 40.0 | 2.0 | 14,9 | 22.8 | 15.6 | | (%) | Imperviousness | Weighted |
| 0.24 | 0.33 | 0.01 | 0.02 | 0.74 | 0.27 | 0.74 | 0.74 | 0,01 | 0.10 | 0.01 | 0.05 | 0.29 | 0.01 | 60.0 | 0.15 | 60.0 | | 1. 199 | 2-Year | OF SO |
| 0.24 | 0.36 | 0.01 | 0.02 | 0,76 | 0.30 | 0,76 | 0,76 | 0,01 | 0.12 | 0,01 | 0.05 | 0.32 | 0.01 | 0.11 | 0,17 | 0.11 | | 11 22 14 | 5-Year | "Runoff Co |
| 1 1 | 0.42 | 0.07 | 0.09 | 0.78 | 0.36 | 0,78 | 0,78 | 0,08 | 0.19 | 0.07 | 0.12 | 0,38 | 0,07 | 0.18 | 0,24 | 0,18 | | | 10-Year | Runoff Coefficient "C" |
| 200 | 0.64 | 0.44 | 0,45 | 0.84 | 0,60 | 0.84 | 0,84 | 0,44 | 0.51 | 0,44 | 0,46 | 0.61 | 0.44 | 0,50 | 0,53 | 0.50 | | • | 100-Year | |

| Land Use | Imperviousness (%) |
|----------------|--------------------|
| Roof | 06 |
| Pavement | 100 |
| Gravel | 40 |
| Landscape/Open | 2 |
| | |

NRCS Hydrologic Soil Group

WEIGHTED PERCENT IMPERVIOUSNESS AND RUNOFF COEFFICIENT "C" Table 1 PENROSE RV & BOAT STORAGE DEVELOPED DRAINAGE J:McCauley Construction 355/355.001.02 Penrose RV Storage/Memos & Reports/Drainage/Spreadsheets/Penrose_DRAINAGE SPREADSHEET_working.xlsx



 ${}^{4}\text{Tt} = (26-17i)+(Lt/(60^{*}(14i + 9)^{*}(\text{So}^{0.5}))) (\text{Eq. 6-5})$ ${}^{3}T_{c} = T_{i} + T_{t} (Eq. 6-2)$

$$\label{eq:transform} \begin{split} ^{1} &Ti = 0.395^{*}(1.1\text{-}C_{5})^{*}L^{05}/S^{0.33} \text{ (Eq. 6-3)} \\ ^{2} &Tt = L/(60^{*}K^{*}(\text{So}^{0.50})) \text{ (Eq. 6-4)} \end{split}$$

| Sub-Basin | Total Area | Overland | Overland Sheet Flow | Shallo | Shallow Concentrated Flow | ted Flow | | • | Eqn 6-3 | | Eqn 6-4 | Eqn 6-4 Eqn 6-2 | |
|---------------|----------------|----------|---------------------|--|---------------------------|--------------------|------|-------|---------|-----------------------|---|-----------------|---------------------------------|
| I.D. | | Length | Slope | Length | Slope | * | Imp | C3 | | 11, | - | 112 | 1t ² Tc ³ |
| Sector 12 | (ac) | (11) | (%) | (ft) | (%) | | (%) | | | (min) | (min) (min) | | (min) (min) (|
| 「ないないないないないない | and an and any | | 「日本の | The Part of the Pa | ALL ALL ALL | The and the second | | 1 180 | | and the second second | The second se | | Selling and |
| 0S-1 | 0.51 | 125 | 6.4% | 152 | 2.4% | 1 | 15.6 | 0.11 | -1 | 10.8 | 10.8 2.3 | | 2.3 |
| OS-2 | 0,40 | 74 | 7.3% | 162 | 0.0% | 7 | 22.8 | 0.17 | - | 7.5 | 7.5 0.0 | _ | 0.0 7.5 |
| 0S-3 | 0.11 | 108 | 4.4% | 0 | 0.0% | 7 | 14.9 | 0.11 | | 11.5 | 11.5 0.0 | | 0.0 |
| SO-1 | 0,12 | 44 | 2.7% | 32 | 0,0% | 15 | 2.0 | 0.01 | | 9.4 | 9.4 0.0 | | 0.0 9.4 |
| SO-2 | 0.02 | 46 | 5.1% | 0 | 0.0% | 20 | 40,0 | 0.32 | | 5.6 | 5.6 0.0 | | 0.0 |
| SO-3 | 0.03 | 21 | 11.1% | 0 | 0.0% | 7 | 8.1 | 0.05 | | 3.9 | 3.9 0.0 | _ | 0.0 |
| SO-4 | 0.02 | 20 | 35.8% | 0 | 0.0% | 7 | 2.0 | 0.01 | | 2.7 | 2.7 0.0 | | 0.0 |
| S-1 | 0.21 | 37 | 1.0% | 318 | 2.8% | 15 | 2.7 | 0.01 | | 11.8 | 11.8 2.1 | | 2.1 |
| S-2 | 0.07 | 40 | 0.0% | 0 | 0.0% | 20 | 90.0 | 0.76 | | 14.1 | 14.1 0.0 | | 0.0 |
| ې ت | 0.14 | 50 | 0.0% | 0 | 0.0% | 20 | 90.0 | 0.76 | | 15.8 | 15.8 0.0 | | 0.0 |
| S4 | 0.48 | 64 | 1.9% | 343 | 2.2% | 20 | 38.3 | 0.30 | | 9.3 | 9.3 1.9 | | 1.9 |
| 5 | 0.20 | 50 | 0.0% | 0 | 0.0% | 20 | 90.0 | 0.76 | | 16.0 | 16.0 0.0 | | 0.0 |
| PND | 0.08 | 34 | 12.3% | 48 | 1.8% | 15 | 4.1 | 0.02 | | 5.0 | 5.0 0.4 | | 0.4 |
| ç | 0.06 | 86 | 5.0% | 0 | 0.0% | 7 | 2.0 | 0.01 | | 10,7 | 10.7 0.0 | 0.0 | - |

NRCS Hydrologic Soil Group

ω

Paved areas and shallow paved swales

20

5 10

Grassed waterway Nearly bare ground Short pasture and lawns

Heavy meadow

Tillage/Field

Type of Land Surface

NRCS Conveyance Factor, K

2.5

сл 7

> PENROSE RV & BOAT STORAGE DEVELOPED DRAINAGE DEVELOPED T_c Table 2





⁴Q = CIA ³I Taken from Final Report OR I = $(28.5*P_{1})/(10+T_{c})^{0.786}$ (Eq. 5-3)

²Table 6-5 (USDCM) along with the weighted imperviousness for each basin was used to find the composite "C" runoff coefficient.

¹P₁ for the 2-year, 5-year, 10-year and 100-year storms were taken from NOAA Attas 14 (Vol. 8, Ver. 2) Point Precipitation Frequency Estimates

1.44

2.01

3.00

9.91

5.60 0.23 0:29

1.38 1.79 **4.31** 0.53 0.45

0.06 0.10 0.08 0.43 0.44 1,71 1.49

0.94

| - | | | _ | | | | | | | | | | | 11. | |
|-----------|------------|------|------|------|------|------|------|------|----------------|------|------|------|------|------|-------|
| lotal | PONDITOTAL | 0-1 | PND | S-5 | S-4 | S-3 | S-2 | S-1 | OFF-SITE TOTAL | SO-4 | SO-3 | SO-2 | SO-1 | US-3 | |
| 2.44 | 1.24 | 0.06 | 0.08 | 0.20 | 0.48 | 0.14 | 0.07 | 0.21 | 1.20 | 0.02 | 0.03 | 0.02 | 0,12 | 0,11 | |
| 10 bearly | 1 | 5.0 | 5.4 | 5.0 | 11.2 | 5.0 | 5,0 | 13.9 | ELSE AVE | 5.0 | 5.0 | 5,0 | 5.0 | 5.0 | |
| 31.0 | 45.0 | 2.0 | 4.1 | 0.06 | 38.3 | 90.0 | 90.0 | 2.7 | 16.5 | 2.0 | 8.1 | 40.0 | 2.0 | 14.9 | |
| 0.21 | 0.33 | 0.01 | 0.02 | 0.74 | 0.27 | 0.74 | 0 74 | 0.01 | 0.10 | 0.01 | 0.05 | 0.29 | 0.01 | 60.0 | |
| 0.24 | 0.36 | 0.01 | 0.02 | 0.76 | 0.30 | 0_76 | 0.76 | 0.01 | 0.12 | 0.01 | 0.05 | 0.32 | 0.01 | 0,11 | |
| 0.31 | 0.42 | 0.07 | 60.0 | 0.78 | 0.36 | 0,78 | 0.78 | 80.0 | 0.19 | 0.07 | 0.12 | 0.38 | 0.07 | 0.18 | |
| 0.57 | 0.64 | 0.44 | 0.45 | 0,84 | 0.60 | 0.84 | 0.84 | 0.44 | 0.51 | 0.44 | 0.46 | 0.61 | 0.44 | 0,50 | |
| | | 2,82 | 2.76 | 2.82 | 2.15 | 2.82 | 2.82 | 1.95 | • | 2,82 | 2,82 | 2.82 | 2.82 | 2.82 | |
| | • | 3.66 | 3.59 | 3.66 | 2,79 | 3.66 | 3.66 | 2,54 | | 3,66 | 3.66 | 3,66 | 3.66 | 3,66 | 0.00 |
| 12/201 | | 4,48 | 4,39 | 4.48 | 3.41 | 4.48 | 4.48 | 3,10 | | 4.48 | 4.48 | 4,48 | 4,48 | 4,48 | |
| 10. 65 | | 8.14 | 7.98 | 8.14 | 6.20 | 8.14 | 8,14 | 5,64 | • | 8.14 | 8.14 | 8,14 | 8,14 | 8,14 | 1140 |
| 1.44 | 1.13 | 0.00 | 0.01 | 0.42 | 0.28 | 0.29 | 0.14 | 0,01 | 0.31 | 0.00 | 0,00 | 0.01 | 0.00 | 0.03 | 0.17 |
| 2.01 | 1.54 | 0.00 | 0.01 | 0.56 | 0.40 | 0.38 | 0,18 | 0,01 | 0.47 | 0,00 | 0,01 | 0.02 | 0.00 | 0.04 | C-2-0 |
| 3.00 | 2.11 | 0.02 | 0.03 | 0,70 | 0.59 | 0,48 | 0.23 | 0.05 | 0.90 | 0.01 | 0.01 | 0.03 | 0.04 | 60.0 | 0,40 |
| | 1200 | | | | | | | | | | | | | | 1 |

PENROSE RV & BOAT STORAGE DEVELOPED PEAK FLOWS DEVELOPED DRAINAGE Table 3

| | 1.32 | 1.08 | 0.83 | Ţ |
|-------------|---------|-------|--------|---|
| ar iuu-year | IU-year | paá.c | z=yeal | |

NRCS Hydrologic Soil Group œ

Sub-Basin I.D.

Total Area

Weighted Imper.

2-Year

5-Year

10-Year

100-Year

²Runoff Coefficient "C"

(ac)

(min) Final T.

(%)

•

ł

•

•

(in/hour) 2-Year

(in/hour) 5-Year

(in/hour) 100-Year

(cfs)

(cfs)

(cfs)

(cfs)

"Rainfall Intensity "I"

10-Year (in/hour)

2-Year

5-Year

10-Year

100-Year

Runoff

OS-2 0S-1

0.40 0.51

5.0 13.1

22.8 15.6

0.15 0.09

0.17 0.11

0.24 0.18

0.53 0.50

2.01

2.61

4.48 3,19

5.80 8,14

0.17 0.10

0.25 0.15

0,43

0.30



| Land Use | Imperviousness (%) |
|----------------------------|--------------------|
| Roof | 90 |
| Pavement | 100 |
| Gravel | 40 |
| Landscape/Open | 2 |
| Historic | 2 |
| NRCS Hydrologic Soil Group | Group B |
| | |

WEIGHTED PERCENT IMPERVIOUSNESS AND RUNOFF COEFFICIENT "C"

PENROSE RV & BOAT STORAGE

Table 4

EXISTING DRAINAGE

Sub-Basin I.D. HOS-2 HOS-3 HOS-1 Total Ч Ч 풊 풍 풍 106,159 21,201 5,326 8,910 17,702 5,406 44,867 2.748 (sf) TOTAL (ac) 2.44 0.49 0.12 1.03 0.20 0.41 0.06 0.12 1,233 (ts) 1,233 0 0 0 0 0 0 Roof 0.00 **0.03** 0.03 0.00 (ac) 5,457 2,323 2,597 537 (sf) 0 0 0 0 Pavement (ac) 0.13 0.05 0.01 0.06 0.00 0_00 0.00 0.00 Area 5,715 (sf) **681** 209 4,666 159 • 0 0 Gravel (ac) 0.00 0.00 0.00 0.11 0.00 (sf) 0 0 0 0 -0 0 LC/Open (ac) 0.00 0.00 0.00 0.00 0.00 93,755 4,580 17,924 5,406 38,968 8,910 (sf) Historic (ac) 0.11 0.20 0.35 0.41 2.15 0.12 0,89 Imperviousness Weighted 10.1 13.4 15.2 2.0 2.0 8.4 (%) 20 15.2 2-Year 0.06 0,09 0,08 0,01 0.01 0.09 0.01 • 5-Year 0.11 0.09 0.01 0,11 0,05 Runoff Coefficient "C" 0.01 0.07 0.01 • 10-Year 0.18 0.16 0.07 0.07 0.18 0.14 0.07 . 100-Year 0,50 0,49 0.44 0.44 0,46 0.44 •

¹Runoff Coefficient "C" Values are from Table 6-5 in the USDCM,

CIVIL RES DURCES



¹Ti = $0.395*(1.1-C_5)*L^{0.5}/S^{0.33}$ (Eq. 6-3)

| HO-1 | HOS-3 | HOS-2 | HOS-1 | H-3 | H-2 | 포 | Constraint of the second | の日本の | ē | Sub-Basin |
|------|-------|-------|-------|------|------|------|--------------------------|-------|--|---------------------------|
| 0.06 | 0.12 | 0.49 | 0.41 | 0.20 | 1.03 | 0.12 | S IN STATES | (ac) | 10 10 10 10 10 10 10 10 10 10 10 10 10 1 | Total Area |
| 76 | 108 | 95 | 85 | 68 | 221 | 258 | Contraction in a | (ft) | Length | Overland |
| 4.8% | 4.3% | 3.3% | 7.4% | 4.1% | 2.9% | 3.5% | 「日の町」日本の | (%) | Slope | Overland Sheet Flow |
| 0 | 0 | 184 | 145 | 0 | 0 | 0 | 大学のなど | (#) | Length | Shallo |
| 0.0% | 0.0% | 2.3% | 3.0% | 0.0% | 0.0% | 0.0% | No. a Stall | (%) | Slope | Shallow Concentrated Flow |
| 7 | 7 | 7 | 7 | 7 | 7 | 7 | | | * | ed Flow |
| 2.0 | 13.4 | 15.2 | 15.2 | 2.0 | 8.4 | 2.0 | ST ALL | (%) | dunb | |
| 0.01 | 0.09 | 0.11 | 0.11 | 0.01 | 0.05 | 0.01 | Statistics of the | の日の湯 | C5 | • |
| 10.2 | 11.6 | 11.8 | 8.5 | 11,6 | 19.7 | 20.9 | | (min) | Ę | Eqn 6-3 |
| 0.0 | 0.0 | 2.9 | 2,0 | 0.0 | 0.0 | 0.0 | | (min) | Tt ² | Eqn 6-4 |
| 10.2 | 11.6 | 14.7 | 10.5 | 11.6 | 19.7 | 20.9 | | (min) | Tc ³ | Eqn 6-2 |
| 0.0 | 0.0 | 25.2 | 24.7 | 0.0 | 0.0 | 0.0 | ALL AND | (min) | Tc4 | Eqn 6-5 |
| 50 | 5.0 | 14.7 | 10.5 | 5.0 | 5.0 | 5.0 | | (min) | Тс | Final |

NRCS Hydrologic Soil Group

ω

Paved areas and shallow paved swales

Nearly bare ground Short pasture and lawns

Tillage/Field Heavy meadow Type of Land Surface

NRCS Conveyance Factor, K

25

Grassed waterway

ਯੋ

10 7 с'n

20

PENROSE RV & BOAT STORAGE EXISTING DRAINAGE EXISTING T_c Table 5



Table 6 PENROSE RV & BOAT STORAGE EXISTING DRAINAGE EXISTING PEAK FLOWS

| | 2-year | 5-year | 10-year | 100-year |
|-----|--------|--------|---------|----------|
| , d | 0.83 | 1.08 | 1,32 | 2 |

NRCS Hydrologic Soil Group B

| Total | HO-1 | HOS-3 | HOS-2 | HOS-1 | H-3 | H-2 | £ | こうべきいいのない | の人口のないない。 | Б. | Sub-Basin |
|--|------|-------|-------|-------|------|------|------|--|-----------|----------|--|
| 2.44 | 0.06 | 0.12 | 0.49 | 0.41 | 0.20 | 1.03 | 0.12 | AND TONS | (ac) | | Total Area |
| 1- | 5.0 | 5.0 | 14.7 | 10.5 | 5.0 | 5.0 | 5.0 | The state of the s | (min) | · · e | Final |
| 10.1 | 2.0 | 13.4 | 15.2 | 15.2 | 2.0 | 8.4 | 2.0 | Participant of the second s | (%) | Imper. | Welghted |
| 0.06 | 0.01 | 80.0 | 0.09 | 0.09 | 0.01 | 0.05 | 0.01 | 1 2 2 7 2 | 1000 | 2-Year | 10 - 2 - 2 17 |
| 0.07 | 0.01 | 60.0 | 0.11 | 0,11 | 0.01 | 0.05 | 0.01 | 「二、二、二、二、二、二、二、二、二、二、二、二、二、二、二、二、二、二、二、 | 11.00 | 5-Year | ² Runoff Co |
| 0.14 | 0.07 | 0_16 | 0,18 | 0.18 | 0.07 | 0.12 | 0.07 | The second | | 10-Year | ² Runoff Coefficient "C" |
| 0.47 | 0.44 | 0.49 | 0.50 | 0.50 | 0.44 | 0,46 | 0.44 | The second | | 100-Year | |
| | 2.82 | 2.82 | 1.91 | 2.20 | 2.82 | 2.82 | 2.82 | THE OWNER | (In/hour) | 2-Year | |
| | 3.66 | 3.66 | 2,48 | 2.86 | 3.66 | 3.66 | 3,66 | | (in/hour) | 5-Year | ³ Rainfall Intensity |
| | 4.48 | 4.48 | 3.03 | 3.50 | 4.48 | 4,48 | 4.48 | arean . | (in/hour) | 10-Year | Intensity "I" |
| 11.75.280 | 8,14 | 8,14 | 5.51 | 6.36 | 8.14 | 8,14 | 8.14 | | (in/hour) | 100-Year | 5.5. 8.6 |
| 0.34 | 0.00 | 0.03 | 0.08 | 0.08 | 0.01 | 0.14 | 0.00 | | (cfs) | 2-Year | |
| 0.52 | 0.00 | 0.04 | 0,13 | 0,13 | 0.01 | 0,20 | 0.00 | Rolling . | (cfs) | 5-Year | 42 |
| 1.31 | 0.02 | 0.09 | 0.27 | 0,26 | 0.06 | 0.57 | 0.04 | 2-20 | (cfs) | 10-Year | 'Runoff |
| 8,40 | 0.23 | 0.49 | 1,34 | 1,29 | 0.73 | 3.87 | 0.44 | ALC: NO | (cfs) | 100-Year | 1997 - 19 |

¹P, for the 2-year, 5-year, 10-year and 100-year storms were taken from NOAA Atlas 14 (Vol. 8, Ver. 2) Point Precipitation Frequency Estimates

²Table 6-5 (USDCM) along with the weighted imperviousness for each basin was used to find the composite "C" runoff coefficient, ³I Taken from Final Report OR I = $(28.5^{\circ}P_{I})/(10+T_{..})^{0.76}$ (Eq. 5-3)

⁴Q = CIA

CIVIL RES SURCES

Overall Site Total Direct Off-Site

HOS-2

HOS-1

Total

HOS-3

Total

Detention Pond

H-2

H-2

HO-1



Table 7

PENROSE RV & BOAT STORAGE SITE

RUNOFF COMPARISON

Point of Discharge

Basin

2-Year 5-Year 10-Year

100-Year

Basin

2-Year 5-Year 10-Year

100-Year

2-Year

5-Year 10-Year

100-Year

2-Year

5-Year

10-Year

100-Year

∆ in Discharge from Discharge Point Proposed LESS Existing (CFS)

Proposed (CFS)

Proposed (CFS)

Runoff

Total Site Discharge

Existing (CFS)

Runoff

Ξ

APPENDIX C

Hydraulic Computations

5/15/2024, 4:29 PM

Penrose_MHFD-Detention_v4-06_2024-05-13.vtsm, Basin

| 0.102 | Select Zone 3 Storage Volume (Optional) = acre-feet | Zone 2 Volume (100-year - Zone 1) = 0.083 acre-feet | 0.020 | 1 | | Approximate rou-yr betention volume = 0.102 acre-feet | 0.086 | 0.0// | 0.062 | 0.044 | 0.031 | 0.287 | 0.180 acre-feet | | Г | 10-yr Runoff Volume (P1 = 1.32 in.) = 0.064 acre-feet 1.32 inches | | 2-yr Runoff Volume (P1 = 0.83 in.) = 0.033 acre-feet 0.83 inches | Excess Urban Runoff Volume (EURV) = 0.059 acre-feet acre-feet | Water Quality Capture Volume (WQCV) = 0.020 acre-feet acre-feet | die einverveel colorado urban hydrograph Procedure. Optional User Overrides | | After providing required inputs above including 1-hour rainfall | Location for 1-hr Rainfall Depths = User Input | Target WQCV Drain Time = 40.0 hours | Percentage Hydrologic Soil Groups C/D = 0.0% percent | Percentage Hydrologic Soil Group B = 100.0% percent | Percentage Hydrologic Soil Group A = 0.0% percent | Watershed Imperviousness = 45.00% percent | Watershed Slope = 0.020 N/A | Watershed Length to Centroid = 240 ft | 450 | Watershed Area = 1.24 acres | Selected BMP Type EDB | Watershed Information | Example Zone Configuration (Retention Pond) | ZONE 1 AND 2 UNITIVE | | YOUNE ENNY WOOV | Jackes Jackes | ri ujevi: relitose kv & boat storage | | DETENTION BASIN STAGE-STORAGE - | |
|-------|---|---|-------|----|---|---|-------|-------|-------|-------|-------|-------|-----------------|----|-----|---|----|--|---|---|---|---|---|--|-------------------------------------|--|---|---|---|-----------------------------|---------------------------------------|--------|-----------------------------|------------------------|-----------------------|---|----------------------|-------------------|-----------------|---------------|--------------------------------------|--|---------------------------------|--|
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 5506 | 5505.5 | 5505 | 5504.5 | 5504 | 5503.5 | Top of Micropool | Stage - Storage Description | Debot trickenter - | Donth Increment = | | | | MHFD-Detention, Version 4.06 (July 2022) | SIN STAGE- | |
| 1 | 3 | 1 | a | ï | 1 | 1 | Ē | T | £ | 1 | ŧ | Ŭ. | £ | 1 | L | ä | Ē | 1 | ī | à | 1 | á | I | a | 1 | + | 1 | P | 1 | 10 | 1 | ı | 1 | 1 | F | Stage (ft) | | | | | | on 4.06 (Ju | TORA | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 3.00 | 2.50 | 2.00 | 1.50 | 1.00 | 0.50 | 0.00 | Override Stage (ft) | Optional | • | | | | uly 2022) | | |
| r | 1 | 1 | 1 | r | 9 | | 1 | 1 | : | 4 | | ÷ | (f .) | i. | 222 | 1 | t) | ji | E. | (į | ï | 1 | r | | ï | ă | ŧ | 1 | 1 | a) | : | 6 | , | ŭ. | È | Length (ft) | | | | | | | | |
| I. | 1 | 220 | | r. | 3 | 1 | | ŧ | 1 | | ł | 1 | (t) | ł | t. | | ц. | | | 1 | 1 | 3 | £ | ių. | ŧ | 17 | ĩ | ġ | ŧ | | , | Ŕ | , | ; | 1 | (ft) | | | | | | | | |

| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 5506 | 5505.5 | 5505 | 5504.5 | 5504 | 5503.5 | Top of Micropool | Stage - Storage Description |
|---|----|---|----|---|---|---|------------------|----|---|---|---|-----|--------------|---|-------------|---|------------|---|---|------------|----|---|---|----|----|----|----|---|-------|--------|-------|-------------|-------|--------|------------------|---|
| 1 | ġ. | ī | a) | 1 | 1 | 1 | Ē |)î | 1 | 1 | ŧ | ĴŦ, | 1 | 1 | Ľ | â | ŕ | 1 | i | ŝ. | ī | a | I | а | 1 | 4 | 1 | P | 1 | B | 4 | 1 | 1 | 1 | F | Stage (ft) |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 3.00 | 2.50 | 2.00 | 1.50 | 1.00 | 0.50 | 0.00 | Optional Override Stage (ft) |
| ŝ | 1 | I | 0 | r | 2 | : | 31. ⁻ | i | 4 | ġ | ŧ | į. | (i ; | 1 | 100 | T | ¥) | â | r | (i | ¥. | 9 | £ | 9 | î. | ä | \$ | 1 | t | æ | 1 | 2 0/ | 3 | ž | ĩ | Length (ft) |
| | 1 | Ľ | 1 | ı | 3 | t | 2 | * | a | : | ł | : | (1) | 1 | (1) | • | | a | t | 1 | T. | 4 | £ | S# | ŧ | | Ŧ | ġ | ŧ | : | ï | Ŕ | ¥ | | 1 | (ft) |
| | 1 | Ŀ | • | | 4 | ı | 1 | ŗ | 1 | ł | 1 | 1 | 3 | * | | 1 | 1 5 | 1 | 1 | • | 15 | | £ | 1 | E. | i, | ŧ | | 1 | 3 | ĸ | 36 | 9 | ÷. | 1 | Area (ft ²) |
| | | | | | | | | | | | | | | | - | | | | | | | | | | | | | | 3,776 | 3,013 | 2,454 | 2,026 | 1,384 | 353 | 0 | Optional Override Area (ft ²) |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 0.087 | 690"0 | 0.056 | 0.047 | 0.032 | 0.008 | 0.000 | Area (acre) |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 5,559 | 3,862 | 2,495 | 1,375 | 522 | 88 | | Valume (ft ³) |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 0.128 | 0.089 | 0,057 | 0.032 | 0.012 | 0.002 | 1.125 | Volume (ac-ft) |

| | D | | BASIN OU | | | SIGN | - | | |
|---|--|--|--|---|---|---|---|---|---|
| | Penrose RV & Bo | at Storage | MHFD-Detention, | Version 4.06 (July | 2022) | | | | |
| Basin ID | PND | | | | | | | | |
| (Tome + | - | | | Estimated | Estimated | | | | |
| | all | | | Stage (ft) | Volume (ac-ft) | Outlet Type | - | | |
| T with Make | 1 8 | | Zone 1 (WQCV | | 0.020 | Drifice Plate | | | |
| POINTANEUT ORIFICES | IDSYEAN | | Zone 2 (100-year | 2_70 | 0.083 | Weir&Pipe (Restrict |) | | |
| | e Configuration (P | Intention Rond) | Zone | 3 | | | | | |
| | | | | Total (all zones | 0_102 | J | FL. | | |
| User Input: Orifice at Underdrain Outlet (typica Underdrain Orifice Invert Depth = | | | | | | | | eters for Underdrain | 1 |
| Underdrain Orlifice Diameter | | inches | the filtration media | a surface) | | drain Orifice Area = | | R' | |
| | | Jaiches | | | Underdrai | n Orifice Centroid = | N/A | feet | |
| User Input: Orifice Plate with one or more orifi | ces or Elliptical Slot | Weir (typically use | d to drain WOCV an | vi/or FURV In a sed | mentation BMD1 | | Cale dated in | | |
| Centroid of Lowest Orifice = | 0.00 | It (relative to basi | n bottom at Stage : | = 0 ft) | | ice Area per Row | Calculated Parame 8.333E-04 | n ² | |
| Depth at top of Zone using Orifice Plate = | 1.23 | | n bottom at Stage : | | | iptical Half-Width | | feet | |
| Orifice Plate: Orifice Vertical Spacing = | 5.50 | inches | | | | ical Slot Centroid = | | feet | |
| Orifice Plate: Orifice Area per Row = | 0.12 | sq. inches (diame | ter = 3/8 inch) | | | Iliptical Slot Area | the second se | rt2 | |
| | | | | | | | | | |
| | | | | | | | | | |
| User Input: Stage and Total Area of Each Orific | | | | | | | | | |
| Characterization of the second | Row 1 (required) | | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Rew 6 (optional) | Row 7 (optional) | Row 8 (optional) | |
| Stage of Orifice Centroid (ft Orifice Area (sg. inches | - | 0.50 | 1.00 | | | | 1 | | |
| Unifice Area (sq. inches) | 0.12 | 0.12 | 0.12 | | | | | | 1 |
| | Row 9 (optional) | Row 10 (optional) | Pour 11 Jonting-IN | Row 12 (college 1) | Days 12 (1997) | | La | 1 | 1 |
| Stage of Orifice Centroid (ft) | | Now to (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) | - |
| Orifice Area (sq. inches) | | | | | | | | | |
| | | | L | | | | | | |
| User Input: Vertical Orifice (Circular or Rectang | ular) | | | | | | Calculated Parame | sters for Vertical Ori | fice |
| | Not Selected | Not Selected | 1 | | | | Not Selected | Not Selected | 1 |
| Invert of Vertical Orifice = | | - | ft (relative to basic | n bottom at Stage = | = 0 ft) Ver | tical Orifice Area = | | | n ³ |
| Depth at top of Zone using Vertical Orifice = | | | ft (relative to basir | bottom at Stage = | = 0 ft) Vertica | Orlfice Centroid = | | | feet |
| Vertical Orifice Diameter = | | | inches | | | | | | 12427534 |
| | | | | | | | | | |
| | | | | | | | | | |
| User Input: Overflow Weir (Dropbox with Flat g | | | tangular/Trapezoid | al Weir and No Out | let Pipe) | | Calculated Parame | ters for Overflow W | Veir |
| Overflow Weiz Front Edge Unight Up | Zone 2 Weir | Not Selected | | | | | Zone 2 Weir | Not Selected | |
| Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = | 1.80 | | Iff (relative to basin) | | | | | | - |
| | | | Contraction of the second s | bottom at Stage = 0 | | e Upper Edge, H _t = | 1.80 | | fect |
| Overflow Weir Grate Slope - | 4.00 | | feet | | Overflow W | eir Slope Length = | 1.80 | | feet feet |
| Overflow Weir Grate Slope = Horiz, Lenoth of Weir Sides = | 0.00 | | feet H:V | G | Overflow W ate Open Area / 10 | feir Slope Length = 0-γr Orifice Area = | 4.00 | | feet |
| Horiz. Length of Weir Sides = | 0.00 4.00 | | feet | Gi | Overflow W ate Open Area / 10 verflow Grate Open | /eir Slope Length = 0-γr Orifice Area = Area w/o Debris = | 4.00 | | feet n² |
| Horiz. Length of Weir Sides = Overflow Grate Type = | 0.00 4.00 Type C Grate | | feet H:V | Gi | Overflow W ate Open Area / 10 | /eir Slope Length = 0-γr Orifice Area = Area w/o Debris = | 4.00 | | feet |
| Horiz. Length of Weir Sides = | 0.00 4.00 | | feet H:V | Gi | Overflow W ate Open Area / 10 verflow Grate Open | /eir Slope Length = 0-γr Orifice Area = Area w/o Debris = | 4.00 | | feet n² |
| Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = | 0.00 4.00 Type C Grate 50% | estrictor Plate, or R | feet H:V feet % | Gi | Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Oper | feir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = | 4,00 11.14 5,57 | Elaw Rostriction D | feet n² n² |
| Horiz. Length of Weir Sides = Overflow Grate Type = | 0.00 4.00 Type C Grate 50% | estrictor Plate, or R Not Selected | feet H:V feet % | Gi | Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Oper | feir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = | 4.00 11.14 5.57 s for Outlet Pipe w/ | Flow Restriction PI | feet n² n² |
| Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = | 0.00 4.00 Type C Grate 50% | | feet H:V feet % ectangular Orifice) | Gi | Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Open | feir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = | 4,00 11.14 5,57 | | feet n² n² ate |
| Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = <u>User Input: Outlet Pipe w/ Flow Restriction Plate</u> Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = | 0.00 4.00 Type C Grate 50% (Crcular Orifice, R Zone 2 Restrictor | | feet H:V feet % ectangular Orifice) | G O | Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Open Cal = 0 ft) Ou | feir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = Iculated Parameter | 4.00 11.14 5.57 s for Outlet Pipe w/ | | feet n² n² n² n² |
| Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = <u>User Input: Outlet Pipe w/ Flow Restriction Plate</u> Depth to Invert of Outlet Pipe = | 0.00 4.00 Type C Grate 50% [Circular Orifice, R Zone 2 Restrictor 0.00 | Not Selected | feet H:V feet 96 ectangular Orifice) ft (distance below bz | Gi Oʻ (| Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Open Cal = 0 ft) Ou | feir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = Iculated Parameter utlet Orifice Area = : Orifice Centrold = | 4.00 11.14 5.57 s for Outlet Pipe w/ | | feet n² n² ate |
| Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input; Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = | 0.00 4.00 Type C Grate 50% (Circular Orifice, R Zone 2 Restrictor 0.00 12.00 | Not Selected | feet H:V feet ectangular Onfice) ft (distance below br inches | Gi Oʻ (| Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Open Cal = 0 ft) Ot Outlet | feir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = Iculated Parameter utlet Orifice Area = : Orifice Centrold = | 4.00 11.14 5.57 s for Outlet Pipe w/ | Not Selected | feet n² n² n² R² feet |
| Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or | 0.00 4.00 Type C Grate 50% (Circular Orifice, R Zone 2 Restrictor 0.00 12.00 | Not Selected | reet H:V feet % ecctangular Orifice) ft (distance below bz inches Inches | G O O Ssin bottorn at Stage Half-Cenl | Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Open Cal = 0 ft) Ot Outlet | feir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = Iculated Parameter utlet Orifice Area = : Orifice Centrold = | 4.00 11.14 5.57 s for Outlet Pipe w/ | Not Selected | feet n² n² n² R² feet |
| Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe with Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectanoular or Spillway Invert Stage = | 0.00 4.00 Type C Grate 50% Zone 2 Restrictor 0.00 12.00 Trapecroidal) 2.00 | Not Selected | feet H:V feet ectangular Onfice) ft (distance below br inches | G O O Ssin bottorn at Stage Half-Cenl | Overflow W rate Open Area / 10 verflow Grate Open Dverflow Grate Open Cal = 0 ft) Ot Outlet ral Angle of Restrict Spillway De | eir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = culated Parameter utlet Orifice Area = : Orifice Centrold = tor Plate on Pipe = esign Flow Depth = | 4.00 11.14 5.57 5 for Outlet Pipe w/ Zone 2 Restrictor Calculated Parame | Not Selected | feet n² n² n² R² feet |
| Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe with to Invert of Outlet Pipe Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = | 0.00 4.00 Type C Grate 50% (Circular Orifice, R Zone 2 Restrictor 0.00 12.00 Tracecoidal) 2.00 5.00 | Not Selected | reet H:V feet % ecctangular Orifice) ft (distance below bz inches Inches | G O osin bottorn at Stage Half-Cenl | Overflow W rate Open Area / 10 verflow Grate Open Overflow Grate Open Call = 0 ft) Ot Outlet ral Angle of Restrict Spillway Dr Stage at T | feir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = iculated Parameter utlet Orifice Area = 0 Orifice Centroid = tor Plate on Pipe = esign Flow Depth= for of Freeboard = | 4.00 11.14 5.57 s for Outlet Pipe w/ Zone 2 Restrictor Calculated Paramet 0.27 3.27 | Not Selected N/A | feet n² n² n² R² feet |
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| Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe with the Invert of Outlet Pipe Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectanoular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Encuted Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Rhuoff Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) Predevelopment Unit Peak Niflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q (cfs) = Ratio Peak Cutflow to Predevelopment Q (cfs) = Ratio Peak Cutflow to Predevelopment Q (cfs) = Nax Velocity through Grate 1 (fps) Max Velocity through Grate 2 (fps) Time to Drain 97% of Inflow Volume (hours) = | 0.00 4.00 Type C Grate 50% (Circular Orifice, R 2one 2 Restrictor 0.000 12.00 12.00 12.00 5.00 4.00 1.00 5.00 4.00 1.00 1.00 1.00 1.00 1.00 1.00 1 | Not Selected It (relative to basin feet H:V feet EURV N/A 0.059 N/A | feet H:V feet feet % ectangular Orifice) ft (distance below ba inches loches bottom at Stage = # hydrographs and 2 Year 0.83 0.033 0.033 0.033 0.033 0.033 0.033 0.04 0.4 0.012 N/A Plate | G O O O O O thalf-Cent Half-Cent 0 ft) 1 runoff volumes by 5 Year 1.08 0.016 0.046 0.046 0.046 0.046 0.05 0.5 0.5 0.013 0.0 Plate | Overflow Weir 1 | feir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = n Area w/ Debris = culated Parameter utlet Orifice Area = 0-rifice Centroid = tor Plate on Pipe = esign Flow Depth= for of Freeboard = op of Freeboard = op of Freeboard = op of Freeboard = sin the Inflow Hyr 25 Year 1.70 0.106 0.106 0.6 0.6 0.45 1.4 0.94 1.7 0.94flow Weir 1 | 4.00 11.14 5.57 5.57 5.57 5.57 5.57 5.57 5.57 2.00 2.20 2.20 2.27 3.27 0.09 0.13 6.27 3.27 0.09 0.13 6.27 3.27 0.09 0.13 6.27 3.27 0.09 0.13 6.27 3.27 0.09 0.13 6.28 5.57 6.27 1.27 0.09 0.13 6.27 1.28 1.28 1.28 1.28 1.28 1.50 1.8 0.09 1.8 0.09 1.8 0.09 1.8 0.9 1.8 0.09 1.8 0.09 1.8 0.09 1.8 0.09 1.8 0.09 1.8 0.09 1.8 0.09 1.8 0.09 1.8 0.09 1.8 0.09 1.8 0.09 1.8 0.09 1.8 0.09 1.8 0.09 1.8 0.09 1.8 0.09 1.8 0.09 1.8 0.08 1.8 0.09 1.8 0.00 1.8 0.00 1.8 0.00 1.8 0.00 1.8 0.00 1.8 0.00 | Not Selected N/A N/A ters for Spillway feet acres acres acre-ft 100 Year 2.40 0.180 1.2 10.49 8.46 2.3 2.16 0.2 Overflow Weir 1 0.0 N/A | feet feet ft ² ft ² feet radians |
| Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe with the structure Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectanoular or Spillway Invert Stage = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Reuted Hydrograph Volume (accert) Inflow Hydrograph Volume (accert) CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) Predevelopment Unit Peak Flow, q (cfs) Predevelopment Unit Peak Flow, q (cfs) Peak Inflow Q (cfs) Peak Outflow to Predevelopment Q (cfs) Ratio Peak Outflow to Predevelopment Q (cfs) Max Velocity through Grate 1 (fps) Max Velocity through Grate 2 (fps) Time to Drain 97% of Inflow Volume (hours) Time to Drain 97% of Inflow Volume (hours) | 0.00 4.00 Type C Grate 50% [Circular Orifice, R Zone 2 Restrictor 0.00 12.00 Traperoidal) 2.00 5.00 4.00 1.00 The user can over WQCV N/A N/A N/A N/A N/A N/A N/A N/A | Not Selected It (relative to basin feet H:V feet EURV N/A 0.059 N/A | feet H:V feet 96. ectangular Orifice) ft (distance below ba- inches Inches I bottom at Stage = 10 bot | G O O O O C Assin bottom at Stage Half-Cent U Half-Cent 0 ft) 0 ft) 0 ft) 0 ft) 0 ft) 0 ft 0 ft 0 ft 0 ft 0 ft 0 ft 0 ft 0 ft | Overflow W ate Open Area / 10 verflow Grate Open verflow Grate Open verflow Grate Open Selflow Grate Open Spillway Du Stage at T Basin Area at T Basin Area at T Basin Area at T Basin Area at T Basin Volume at T entering new volue 10 Year 1.32 0.064 0.1 3.24 0.064 0.1 3.24 0.064 0.1 0.260 0.1 0.260 0.1 0.260 0.1 0.260 0.1 0.7 0.1 0.7 0.1 0.260 0.1 0.7 0.1 0.7 0.1 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 | feir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = n Area w/ Debris = culated Parameter utlet Orifice Area = 0 orifice Centroid = tor Plate on Pipe = esign Flow Depth= op of Freeboard = op of Freeboard = op of Freeboard = op of Freeboard = op of Freeboard = on 0.106 0.106 0.6 - - 0.45 1.4 0.94 1.7 Overflow Weir 1 0.0 N/A | 4.00 11.14 5.57 5.57 20ne 2 Restrictor Calculated Paramet 0.27 3.27 0.09 0.13 6.09 0.138 0.068 1.50 1.8 0.00 0.138 0.00 0.00 0.138 0.00 0.00 0.138 0.00 0.00 0.138 0.00 0.00 0.138 0.00 0.00 0.00 0.138 0.00 0.00 0.00 0.138 0.00 0.00 0.00 0.138 0.00 0.00 0.00 0.138 0.00 0 | Not Selected N/A N/A ters for Spillway feet feet acres acre-ft lumns W through A 100 Year 2.40 0.180 1.2 10.49 8.46 2.3 2.16 0.2 Overflow Weir 1 0.0 | feet feet ft ² ft ² feet radians |
| Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe with the Invert of Outlet Pipe Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectanoular or Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Restrictor Plate Height Above Pipe Invert stage= Spillway End Slopes = Freeboard above Max Water Surface = Restrict Plate Height Restrict (in) CUHP Predevelopment Peak Q (cfs) = Predevelopment Peak Q (cfs) Predevelopment Q (cfs) = Peak Julfow Q (cfs) = Peak Julfow D Predevelopment Q (cfs) = Ratio Peak Outflow to Predevelopment Q (cfs) Max Velocity through Grate 1 (fps) Max Velocity through Grate 1 (fps) Time to Drain 99% of Inflow Volume (hours) = Time to Drain 99% of Inflow Volume (hours) = | 0.00 4.00 Type C Grate 50% Zone 2 Restrictor 0.00 12.00 Traccroidal 2.00 5.00 4.00 1.00 The user can over WQCV N/A 0.020 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A | Not Selected R (relative to basin feet H:V feet EURV N/A N/A N/A N/A N/A N/A N/A N/A N/A Spillway 0.000 N/A 63 68 2.04 | feet H:V feet feet feet feet feet f(distance below ba inches bottom at Stage = <i>P hydrographs and</i> 2 Year 0.83 0.033 0.033 0.033 0.033 0.033 0.033 0.033 0.033 0.033 0.033 0.033 0.033 0.04 0.4 0.012 N/A Plate N/A N/A 53 56 1.48 | G O O O Half-Cent Half-Cent 0 ft) 1.08 0.046 0.046 0.046 0.046 0.046 0.046 0.046 0.046 0.046 0.046 0.046 0.05 0.05 0.013 0.0 Plate N/A N/A 63 68 1.74 | Overflow W ate Open Area / 10 verflow Grate Open Overflow Grate Open Overflow Grate Open Overflow Grate Open Cal = 0 ft) Ou Stage at Spillway Du Stage at T Basin Area at T Basin Area at T Colored 0.064 0.064 0.1 3.24 2.61 0.8 0.260 0.1 Overflow Weir 1 0.0 N/A 64 70 70 1.84 | feir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = n Area w/ Debris = culated Parameter utlet Orifice Area = 0 orifice Centroid = tor Plate on Pipe = esign Flow Depth= op of Freeboard = op of Freeboard = 0 of Streeboard = 0 0.106 0.106 0.6 - - 0.45 1.4 0.94 1.7 Overflow Weir 1 0.0 N/A 60 68 1.91 | 4.00 11.14 5.57 5.57 5.57 5.57 5.57 2.00 2.00 2.27 3.27 0.09 0.13 6.27 3.27 0.09 0.13 6.09 0.13 6.138 0.138 0.138 0.138 0.138 0.138 0.138 0.138 0.138 0.138 0.138 0.138 0.138 0.138 0.59 1.8 1.50 1.8 1.50 1.8 1.50 1.8 1.50 1.8 1.50 1.8 1.57 1.65 1.8 1.57 1.8 1.8 1.57 1.8 1.57 1.8 1.57 1.8 1.8 1.8 1.8 1.95 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8 | Not Selected N/A ters for Spillway feet feet acres acreft 100 Year 2.40 0.180 0.180 1.2 10.49 8.46 0.2 Overflow Weir 1 0.0 N/A 54 64 1.99 | feet feet ft ² ft ² feet feet radians |
| Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe with the structure Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectanoular or Spillway Invert Stage = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Reuted Hydrograph Volume (accert) Inflow Hydrograph Volume (accert) CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) Predevelopment Unit Peak Flow, q (cfs) Predevelopment Unit Peak Flow, q (cfs) Peak Inflow Q (cfs) Peak Outflow to Predevelopment Q (cfs) Ratio Peak Outflow to Predevelopment Q (cfs) Max Velocity through Grate 1 (fps) Max Velocity through Grate 2 (fps) Time to Drain 97% of Inflow Volume (hours) Time to Drain 97% of Inflow Volume (hours) | 0.00 4.00 Type C Grate 50% [Circular Orifice, R Zone 2 Restrictor 0.00 12.00 Traperoidal) 2.00 5.00 4.00 1.00 The user can over WQCV N/A N/A N/A N/A N/A N/A N/A N/A | Not Selected It (relative to basir feet H:V feet EURV N/A 0.059 N/A | feet H:V feet 96. ectangular Orifice) ft (distance below ba- inches Inches I bottom at Stage = 10 bot | G O O O O C Assin bottom at Stage Half-Cent U Half-Cent 0 ft) 0 ft) 0 ft) 0 ft) 0 ft) 0 ft 0 0.046 0.046 0.046 0.046 0.046 0.046 0.046 0.013 0.0 Plate N/A N/A N/A N/A 63 68 | Overflow W ate Open Area / 10 verflow Grate Open verflow Grate Open verflow Grate Open Selflow Grate Open Spillway Du Stage at T Basin Area at T Basin Area at T Basin Area at T Basin Area at T Basin Volume at T entering new volue 10 Year 1.32 0.064 0.1 3.24 0.064 0.1 3.24 0.064 0.1 0.260 0.1 0.260 0.1 0.260 0.1 0.260 0.1 0.7 0.1 0.7 0.1 0.260 0.1 0.7 0.1 0.7 0.1 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 | feir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = Indiated Parameter Indiated Parameter utlet Orifice Area = Orifice Centrold = tor Plate on Pipe = esign Flow Depth = op of Freeboard = op of Freeboard = op of Freeboard = 0.06 0.6 0.45 1.4 0.94 1.7 Overflow Weir 1 0.0 N/A 60 68 | 4.00 11.14 5.57 5.77 | Not Selected N/A ters for Spillway feet feet acres acre-ft 100 Year 2.40 0.180 1.2 10.49 8.46 2.3 2.16 0.2 Overflow Weir 1 0.180 4.46 64 | feet n ² n ² n ² feet radians 500 Year 3.43 0.287 0.287 2.1 1.68 3.6 3.7 1.8 Spillway 0.0 N/A 48 61 |



DETENTION VOLUME BY THE MODIFIED FAA METHOD

Project: Penrose RV & Boat Storage

Basin ID: PND

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(For catchments less than 160 acres only. For larger catchments, use hydrograph routing method) (NOTE: for catchments larger than 90 acres, CUHP hydrograph and routing are recommended)

| | | | tention Volun | we Using Modi | fied FAA Meth | hod | Determination of MAJOR Detention Volume Using Modified FAA Method | | | | | | | |
|---|---|------------------------------------|--|-------------------------------|---|-----------|---|------------------|-------------------|---|--------------|----------------|---------|--|
| Calchment Dra Calchment Dra Return Period I Time of Conce Mowable Unit Doe hour Preci Design Rainfa Coefficient Oni Coefficient Two | Design Information (Input): mem Drainage Area Design Information (Input): Cathment Drainage Imperiousness Is = 45.00 Is = 45.00 percent mem Drainage Area A = 1240 acres Cathment Drainage Imperiousness A = 1240 acres wolopment NRCS Soil Group Type = B A, B, C, or D Predevelopment NRCS Soil Group Type = B A, B, C, or D Prend for Delenion Convol T = 100 years (2, 5, 10, 25, 50, or 100) Return Prind P | | | | | | | | | acres A. B, C, or D years (2, 5, 10, minutes cfs/acre | | | | |
| demolent mi | 88 | | C3 | 0.789 | J | | Coefficient Th | nee | | C | 0.789 | | | |
| Determinati Runoff Coeffici nflow Peak Ru kilowable Peak | notf Outflow Rate Mor Mor | d. FAA Minor SI d. FAA Minor SI | C = Op-in = Op-oul = Iorage Volume = Iorage Volume = | 0,38 2,09 0,29 1,718 | cls cls cubic feet acre-ft 5-Marufes) | | Determination of Average Outflow from the Basin (Calculated): Runolf Coefficient C = 0.51 Inflow Peak Runolf Op-in = 5.11 cfs Allowable Peak Outflow Rale 0.004 1.05 cfs Mod, FAA Major Storage Volume = 3.402 cubic feet Mod, FAA Major Storage Volume = 0.076 acre-11 | | | | | | | |
| RainIall | Rainfalt | Inflow | Adjustment | Average | Outflow | Storage | Rainfall | Rainfall | Inflow | Adjustment | Average | Outflow | Storag | |
| Duration minutes | Intensity inches / hr | Volume acreiteet | Factor | Out!low | Volume | Volume | Duration | Intensity | Volume | Factor | Outflow | Volume | Volum | |
| (ipout) | (output) | (output) | "m" (outout) | cfs (output) | acre-feet | acro-feet | minules | inches / hr | acro-feet | "m" | cls | acra-feet | acre-fe | |
| 5 | 4.44 | 0.014 | 1.00 | (output) 0.29 | (oulput) 0.002 | 0.012 | (input) 5 | (oulput) 8.07 | (output) 0.035 | (oulput) | (output) | (output) | (oulpi | |
| 10 | 3,54 | 0.023 | 0.75 | 0.21 | 0.002 | 0.020 | 10 | 6.43 | 0.035 | 1.00 | 1.05 | 0.007 | 0.028 | |
| 15 | 2.97 | 0.029 | 0.67 | 0.19 | 0.004 | 0.025 | 15 | 5.40 | 0.071 | 0.67 | 0.79 | 0.011 | 0.04 | |
| 20 25 | 2.57 | 0.033 | 0.63 | 0.16 | 0.005 | 0.028 | 20 | 4.67 | 0.081 | 0.63 | 0.66 | 0.018 | 0.06 | |
| 30 | 2.28 | 0.037 | 0.60 | 0.17 | 0.006 | 0.031 | 25 | 4.14 | 0.090 | 0.60 | 0.63 | 0.022 | 0.06 | |
| 35 | 1.87 | 0.042 | 0.58 | 0.17 | 0.007 | 0.033 | 30 | 3.72 | 0.097 | 0.58 | 0.61 | 0.025 | 0.07 | |
| 40 | 1.72 | 0.045 | 0.56 | 0.16 | 0.009 | 0.035 | 40 | 3.39 | 0.103 | 0.57 | 0.60 | 0.029 | 0.07 | |
| 45 | 1.59 | 0.047 | 0.56 | 0.16 | 0.010 | 0.037 | 45 | 2.90 | 0.114 | 0.56 | 0.59 | 0.035 | 0.07 | |
| 50 55 | 1.49 | 0.048 | 0.55 | 0,16 | 0.011 | 0.037 | 50 | 2.70 | 611.0 | 0.55 | 0.58 | 0.040 | 0.07 | |
| 60 | 1.32 | 0.050 | 0.55 | 0.16 | 0.012 | 0.035 | 55 | 2.54 | 0.122 | 0.55 | 0.67 | 0.044 | 0.07 | |
| 65 | 1.25 | 0.053 | 0.54 | 0.15 | 0.013 | 0.039 | 60 65 | 2.39 | 0.125 | 0.54 | 0.57 | 0.047 | 0,07 | |
| 70 | 1.10 | 0.054 | 0.54 | 0.15 | 0.015 | 0.039 | 70 | 2.16 | 0.128 | 0.54 | 0.57 | 0.051 | 0.07 | |
| 75 | 1.13 | 0.055 | 0.53 | 0.15 | 0.016 | 0.039 | 75 | 2.05 | 0.134 | 0.53 | 0.56 | 0.058 | 0.07 | |
| 80 85 | 1.08 | 0.058 | 0.53 | 0.15 | 0.017 | 0.039 | 80 | 1.96 | 0.137 | 0.53 | 0.56 | 0.062 | 0.07 | |
| 90 | 1.04 | 0.057 | 0.53 | 0,15 | 0.018 | 0.039 | 85 | 1.88 | 0.139 | 0.53 | 0.56 | 0.065 | 0.07 | |
| 95 | 0.98 | 0.059 | 0.53 | 0.15 | 0.019 | 0.039 | 90 | 1.81 | 0.142 | 0.53 | 0.56 | 0.069 | 0.07 | |
| 100 | 0.92 | 0.060 | 0.53 | 0.15 | 0.020 | 0.039 | 95 | 1.74 | 0.144 | 0.53 | 0.55 | 0.073 | 0.07 | |
| 105 | 0.89 | 0.061 | 0.52 | 0.15 | 0.022 | 0.039 | 105 | 1.62 | 0.148 | 0.53 | 0.55 | 0.076 | 0.07 | |
| 110 | 0.86 | 0.061 | 0.52 | 0.15 | 0.023 | 0.039 | 110 | 1.57 | 0.150 | 0.52 | 0.55 | 0.083 | 0.06 | |
| 115 | 0.83 | 0.062 | 0.52 | 0.15 | 0.024 | 0.039 | 115 | 1.52 | 0,152 | 0.52 | 0,55 | 0.687 | 0.06 | |
| 125 | 0.78 | 0.063 | 0.52 | 0.15 | 0.025 | 0.038 | 120 | 1.47 | 0.154 | 0.52 | 0.55 | 0.091 | 0.063 | |
| 130 | 0.76 | 0.064 | 0.52 | 0.15 | 0.027 | 0.038 | 125 | 1.43 | 0.155 | 0.52 | 0.55 | 0.094 | 0,06 | |
| 135 | 0.74 | 0.065 | 0.52 | 0.15 | 0.027 | 0.037 | 135 | 1.35 | 0.157 | 0.52 | 0.55 | 0.098 | 0.05 | |
| 140 | 0,72 | 0.065 | 0.52 | 0.15 | 0.028 | 0.037 | 140 | 1.31 | 0,160 | 0.52 | 0.55 | 0.105 | 0.05 | |
| 145 | 0.70 | 0.066 | 0.52 | 0.15 | 0.029 | 0.037 | 145 | 1.28 | 0,162 | 0.52 | 0.55 | 0.109 | 0.053 | |
| 155 | 0.69 | 0.067 | 0.52 | 0.15 | 0.030 | 0.035 | 150 | 1 25 | 0.163 | 0.52 | 0.54 | 0.113 | 0.050 | |
| 160 | 0.65 | 0.068 | 0.52 | 0.15 | 0.031 | 0.036 | 155 | 1.22 | 0.164 | 0.52 | 0.54 | 0.116 | 0.04 | |
| 165 | 0.64 | 0,06# | 0.52 | 0,15 | 0,033 | 0.035 | 165 | 1.19 | 0.166 | 0.52 | 0.54 | 0.120 | 0.044 | |
| 170 | 0.63 | 0.069 | 0.51 | 0.15 | 0.034 | 0.035 | 170 | 1.14 | 0.168 | 0.51 | 0.54 | 0.127 | 0.041 | |
| 175 | 0.61 | 0.069 | 0.51 | 0.15 | 0.035 | 0.034 | 175 | 1,11 | 0.170 | 0.51 | 0.54 | 0.131 | 0.035 | |
| 185 | 0.60 | 0.070 | 0.51 | 0.15 | 0.036 | 0.034 | 180 | 1.09 | 0.171 | 0.51 | 0.54 | 0.134 | 0.034 | |
| 190 | 0.58 | 0.071 | 0.51 | 0.15 | 0.037 | 0.033 | 185 | 1.07 | 0.172 | 0.51 | 0.54 | 0.138 | 0.034 | |
| 195 | 0.56 | 0.071 | 0.51 | 0,15 | 0.039 | 0.032 | 195 | 1.03 | 0.173 | 0.51 | 0.54 | 0.142 | 0.032 | |
| 200 | 0.55 | 0.072 | 0.51 | 0.15 | 0.040 | 0.032 | 200 | 1.01 | 0.175 | 0.51 | 0.54 | 0.149 | 0.023 | |
| 210 | 0.54 | 0.072 | 0.51 | 0.15 | 0.041 | 0.031 | 205 | 0.99 | 0 176 | 0.51 | 0.54 | 0.152 | 0.024 | |
| 215 | 0.52 | 0.073 | 0.51 | 0.15 | 0.042 | 0.031 | 210 215 | 0.97 | 0-177 | 0.51 | 0.54 | 0.156 | 0.021 | |
| 220 | 0.52 | 0.074 | 0,51 | 0.15 | 0.044 | 0.029 | 220 | 0.94 | 0.179 | 0.51 | 0.54 | 0.160 | 0.019 | |
| 225 | 0.51 | 0.074 | 0.51 | 0.15 | 0.045 | 0.029 | 225 | 0.92 | 0.181 | 0.51 | 0.54 | 0.167 | 0.014 | |
| 230 | 0.50 | 0.074 | 0.51 | 0.15 | 0.046 | 850.0 | 230 | 0.91 | 0.181 | 0.51 | 0.54 | 0.171 | 0.011 | |
| 240 | 0.49 | 0.075 | 0.51 | 0.15 | 0.047 | 0.028 | 235 | 0.89 | 0.182 | 0.51 | 0.54 | 0.174 | 0.008 | |
| 245 | 0.47 | 0.076 | 0.51 | 0.15 | 0.049 | 0.026 | 245 | 0.88 | 0.183 | 0.51 | 0.54 | 0.178 | 0.005 | |
| 250 | 0.47 | 0.076 | 0.51 | 0.15 | 0.050 | 0.026 | 250 | 0.85 | 0.185 | 0.51 | 0.54 | 0.181 | 0.003 | |
| 255 | 0.46 | 0.076 | 0.51 | 0.15 | 0.051 | 0.025 | 255 | 0.84 | 0.186 | 0.51 | 0.54 | 0.189 | -0.000 | |
| 260 | 0.45 | 0.077 | 0.51 | 0.15 | 0.052 | 0.025 | 260 | 0.83 | 0.187 | 0.51 | 0.54 | 0.192 | 0.005 | |
| 270 | 0.45 | 0.077 | 0.51 | 0.15 | 0.053 | 0.024 | 265 | 0.81 | 0,188 | 0.51 | 0.54 | 0.196 | 0.008 | |
| 275 | 0.44 | 0.078 | 0.51 | 0.15 | 0.055 | 0.023 | 270 | 0.80 | 0.189 | 0.51 | 0.54 | 0 200 | -0.011 | |
| | 0.43 | 0.078 | 0.51 | 0.15 | 0.056 | 0.022 | 280 | 0.78 | 0,189 | 0.51 | 0.54 | 0.203 | -0.014 | |
| 280 | | | | | | | | | | | | | | |
| 285 | 0.42 | 0.078 | 0.51 | 0.15 | 0.057 | 0.021 | 285 | 0.77 | 0.191 | 0.51 | 0.54 | | | |
| 285 290 | 0.42 | 0.079 | 0.51 | 0.15 | 0.058 | 0.021 | 290 | 0.76 | 0.192 | 0.51 | 0.54 0.54 | 0.211 0.214 | -0.019 | |
| 285 | | | | | | | | | | | 0.54 | 0.211 | -0.019 | |

-0.031 3,402 0.0761

 0.51
 0.14
 0.0660
 0.019
 300
 0.74
 0.193
 0.51
 0.54
 0.221

 0.51
 0.51
 0.54
 0.021
 0.019
 305
 0.73
 0.194
 0.51
 0.54
 0.225

 Mod. FAA Minor Storage Volume (cubic ft.) =
 1,718
 Mod. FAA Major Storage Volume (cubic ft.) =
 0.0384
 Mod. FAA Major Storage Volume (cubic ft.) =
 0.0384
 Mod. FAA Major Storage Volume (cacre-ft.) =
 UDFCD DETENTION BASIN VOLUME ESTIMATING WORKBOOK Version 2.35, Released January 2015

Table 8 PENROSE RV & BOAT STORAGE

STAGE - STORAGE TABLE DETENTION POND

| Stage | Elevation | D Elevation | Area | Incremental Est. Volume | Est. Availa | Est. Available Volume | |
|-------|-----------|---------------------------|----------|-------------------------|-------------|-----------------------|---------------------------------------|
| (11) | (#) | (ft) | (SF) | (CF) | (CF) | (ac-ft) | Note |
| | | 201 420 5 2 3 2 4 2 4 2 4 | 一人の言語のない | | 山、ないに「「「「 | | ····································· |
| 0 | 5503.00 | 0.00 | 0 | 0 | 0 | 0.000 | Outlet Structure Invert |
| 0.50 | 5503.50 | 0.50 | 353 | 88 | 88 | 0.002 | ×. |
| 1.00 | 5504.00 | 0.50 | 1,384 | 434 | 522 | 0.012 | |
| 1.23 | 5504.23 | 0.23 | | | | | WQCV WSEL |
| 1.50 | 5504.50 | 0.50 | 2,026 | 852 | 1,375 | 0.032 | 300) |
| 1.99 | 5504.99 | 0.49 | | | | | 100-yr WSEL |
| 2,00 | 5505.00 | 0.50 | 2,454 | 1,120 | 2,495 | 0.057 | Spillway Invert |
| 2.50 | 5505.50 | 0.50 | 3,013 | 1,367 | 3,862 | 680"0 | • |
| 3.00 | 5506.00 | 0.50 | 3,776 | 1,697 | 5,559 | 0.128 | Top of Berm |







| NOTES: | Project File: | 4 | ω | N | - | No. | Storm |
|--|--------------------------------------|--------------|--------------|--------------|-------------|-------------------------|--------|
| Return period = 100 Yrs. ; *Surcharged (HGL above crown), ; j - Line contains hyd. jump. | ile: 355.001.02_Penrose_100-year.stm | Pipe - (38) | Pipe - (39) | Pipe - (32) | Pipe - (33) | Line ID | Sewer |
| charged (HG | ear.stm | 2.16 | 1.92 | 1,38 | 1.38 | Flow rate (cfs) | |
| L above crow | | 12 | 18 | œ | CO | Line Size (in) | Report |
| vn). <mark>;</mark> j - Lin | | Cir | Cir | Cir | Cir | Line shape | 루 |
| e contains h | | 47 452 | 42 734 | 153.000 | 89,603 | Line length (ft) | |
| <mark>vd: jump.</mark> | | 5502.76 | 5503,35 | 5506.13 | 5505.50 | Invert EL Dn (ft) | |
| | | 5503.00 | 5504.54 | 5509,15 | 5506.13 | Invert EL Up (ft) | |
| | | 0,506 | 2.785 | 1,974 | 0.703 | Line Slope (%) | |
| | Number of lines: 4 | 5503.39 | 5503_87 | 5507,14 | 5506,05* | HGL Down (ft) | |
| | lines: 4 | 5503,75 | 5505.06 | 5509,70 | 5507_11* | (ft) HGL | |
| | | 0.18 | n/a | n/a | 0.04 | Minor loss (ft) | e. |
| | Run | 5503.93 | 5505.06 | 5509.70 j | 5507.14 | HGL Junct (ft) | |
| | Run Date: 5/15/2024 | End | End | <u></u> | End | Dns Line No. | |
| |)24 | OpenHeadwall | OpenHeadwall | OpenHeadwall | Manhole | Junction Type | Page 1 |

Storm Sewers v2025 00

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| NO | Pro | 4 | ω | N | | Τ | Line | Station |
|---|---------------------------------|-------------|-------------|--------------|---------------|---------------|-------|-----------------|
| res:Int | Project File: | End | End | - | End | | To | ion |
| ensity | 355 | | | 153 | | Ē | | Len |
| = 127 | .001.0 | 47.452 (| 42.734 (| 153,000 0.00 | 89.603 0.00 | | _ | |
| 16/(1 | 2_Pen | 0.00 | 0.00 | 0.00 | 0.00 | (ac) | Incr | Drng Area |
| NOTES:Intensity = 127.16 / (Inlet time + 17.80) ^ 0.82; Return period =Yrs. 100 ; c = cir e = ellip b = box | 355.001.02_Penrose_100-year.stm | 0.00 | 0.00 | 0.00 | 0.00 | (ac) | Total | |
| + 17.80 | 0-year.st | 0.00 | 0.00 | 0.00 | 0.00 | (C) | | Rnoff |
|) ^ 0.82; | H | 0.00 | 0.00 | 0.00 | 0.00 | | Incr | Area x C |
| Return | | 0.00 | 0.00 | 0.00 | 0.00 | | Total | Ô |
| period = | | 0.0 | 0.0 | 0.0 | 0.0 | (min) | Inlet | 7 |
| Yrs. 100 | | 0.0 | 0.0 | 0.0 | 0.6 | (min) | Syst | |
| 0 = 0 | | 0.0 | 0.0 | 0.0 | 0.0 | (in/hr) (cfs) | 19 | Rain |
| ir e = e | | 2.16 | 1.92 | 1.38 | 1.38 | (cfs) | 10W | Total |
| lip b = t | | 2,53 | 17.52 | 1.84 | 1.10 | (cfs) | Ē | Cap |
| X | | 3.80 | 3.52 | 4,21 | 4.21 | (ft/s) | | Vel |
| | | 12 | 18 | œ | œ | (in) | Size | Pipe |
| | | 0.51 | 2.78 | 1.97 | 0.70 | (%) | Slope | |
| × | Number | 5502.76 | 5503_35 | 5506 13 | 5505.50 | (ft) | D | Invert Elev |
| | Number of lines: 4 | 5503.00 | 5504.54 | 5509.15 | 5506.13 | (ft) | Up | ev |
| | | 5503.39 | 5503.87 | 5507.14 | 5506.05 | (ft) | Dn | HGL Elev |
| | | 5503 75 | 5505.06 | 5509.70 | 5507.11 | (ft) | dh | ev |
| | Run Date: | 0,00 | 5505.14 | 5508.62 | 0.00 | (ft) | Ŋ | Grnd / F |
| | L I te: 5/15/2024 | 5504.88 | 5506.33 | 2 5511.63 | 5508.62 | (ft) | ų | Grnd / Rim Elev |
| |)24 | Pipe - (38) | Pipe - (39) | Pipe - (32) | 2 Pipe - (33) | | | Line ID |

Page 1

Storm Sewer Tabulation



Proj. file: 355.001.02_Penrose_100-year.stm

Storm Sewer Profile

Storm Sewers



Storm Sewers

Storm Sewer Profile

Proj. file: 355.001.02_Penrose_100-year.stm



Storm Sewer Profile

Storm Sewers

Proj. file: 355.001.02_Penrose_100-year.stm

| | q (cfs/ft) uni | Q (cfs) tota | ³ Q _S (cfs) slopi | ² Q _H (cfs) horizo | S (%) longi | H (ft) head a | L (ft) broad-cr | Z (ft) side slo | ¹ C _{BCW} broad-cres | Parameter Du |
|---------------------------|----------------|-----------------|---|--|--------------------|-----------------------|---------------------------|--------------------------|--|--------------|
| rinran mean narticle size | unit discharge | total discharge | sloping discharge | horizontal discharge | longitudinal slope | head above weir crest | broad-crested weir length | side slopes (horiz:vert) | broad-crested weir coefficient | Description |
| 200 | 1.12 | 5.60 | 0.25 | 5.35 | 10.80 | 0.23 | 5.00 | 4.00 | 3.10 | Value |

 $^{1}C_{BCW}$ ranges 2.6-3.0; 3.0 is typical (USDCM 5.14.2) $^{2}Q=C_{BCW}LH^{1.5}$ (Eq. 12.8 USDCM)

³Q=2(2/5)C_{BCW}ZH^{2.5} (Eq: 12.9 USDCM)

¹d₅₀ (Fig. 12-21 USDCM)



SPILLWAY & RIPRAP SIZING

ngitadinalSicpe (%) ばとはとしました。 ДАБЕЛГ 3 10 8 1,1 0 TYPE VL 13411 NA 39YT (J) TYPE H 10 TYPEVH Unit Discharge (cis/ft) 15 B ы 8

Figure 12-21. Embankment protection details and rock sizing chart (adapted from Arapahec County)

APPENDIX D

Drawings





